University of Twente
The Netherlands

Control Laboratory

Review
Realistic Example

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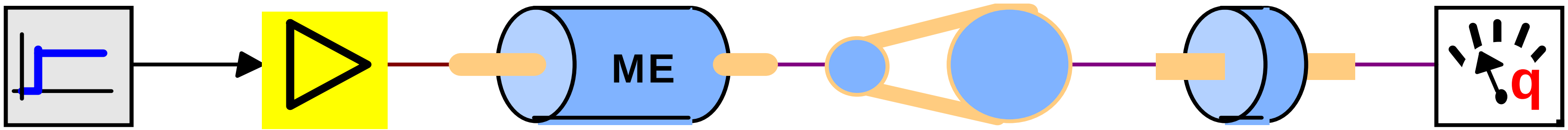
Contents

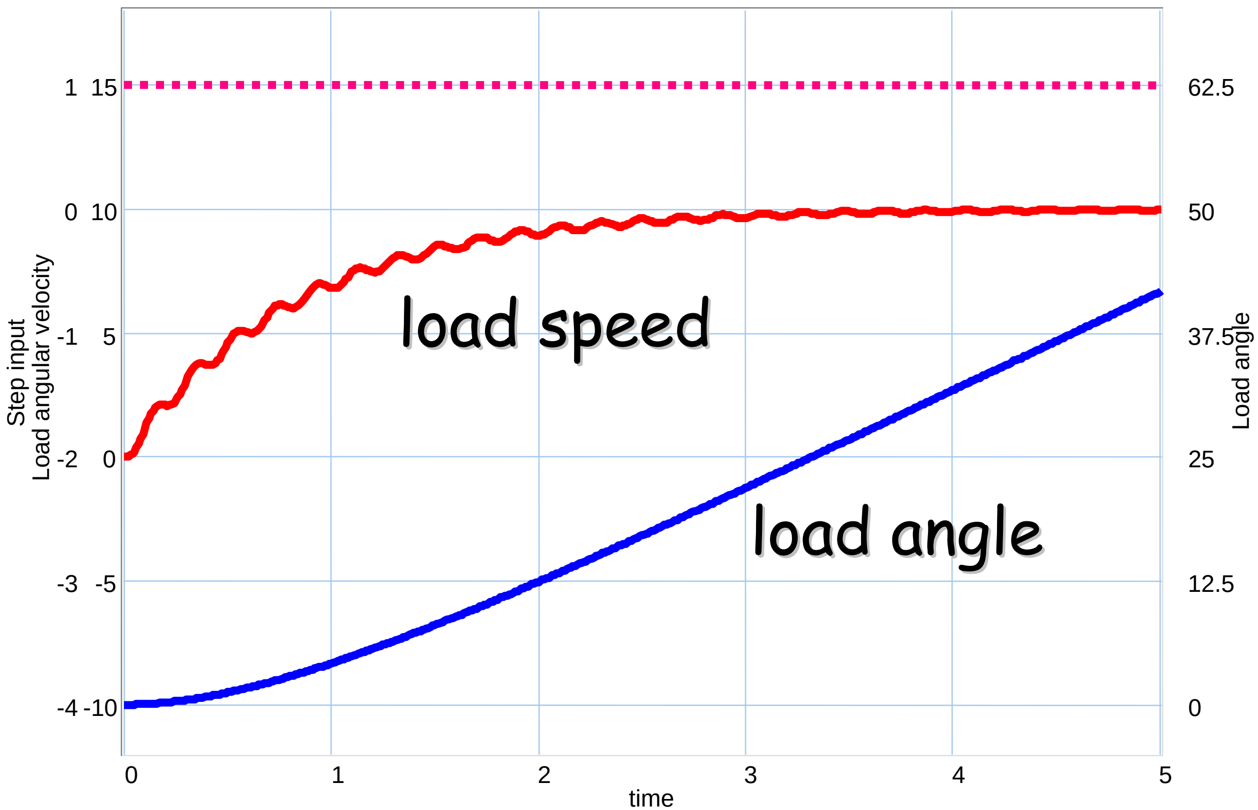
- Design of controllers for a realistic servo system
- Fourth order servo system
  - Tacho feedback

Example of lecture 2



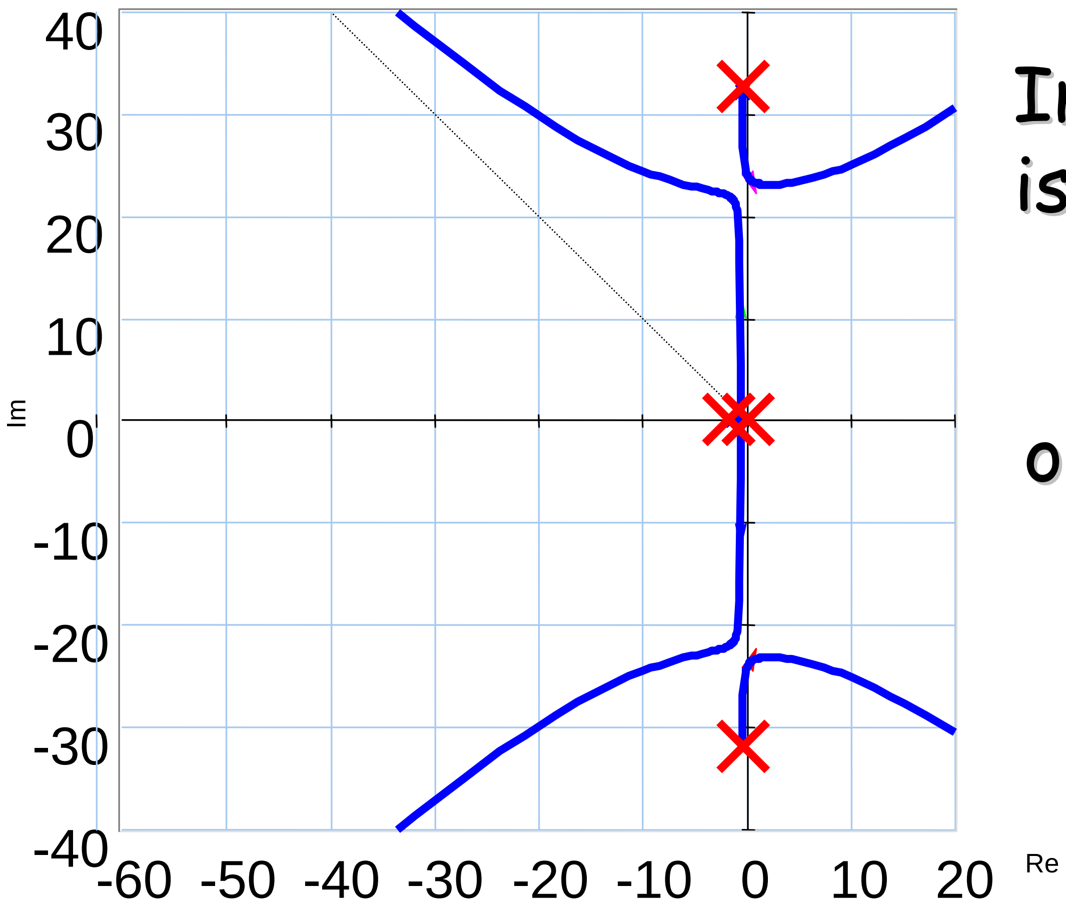
current amplifier | motor | flexible transmission | load | potentio-meter

Example of lecture 2



A_Model_for_identification.em

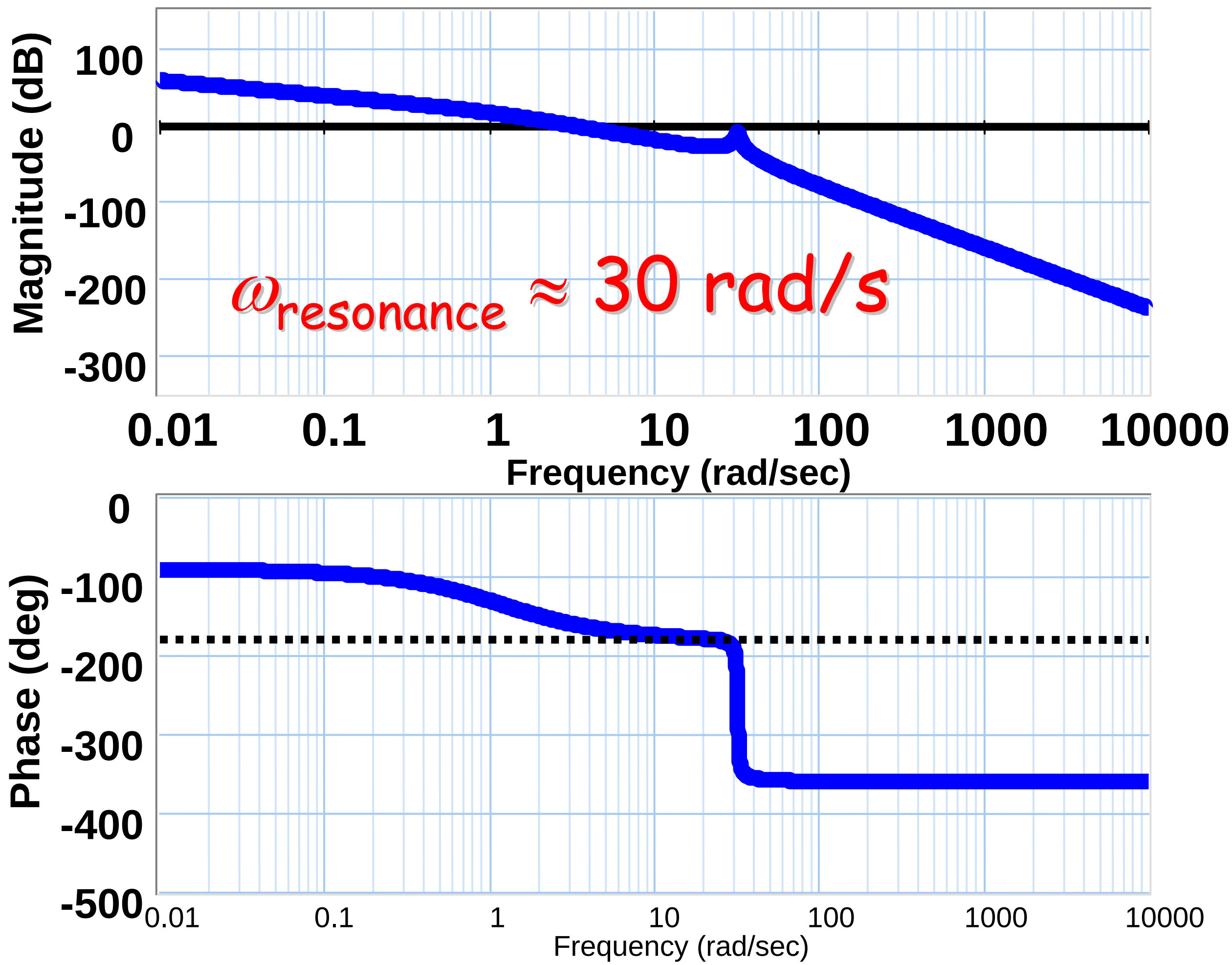
Linearise in 20-sim



In practice this option is not always available:

Black Box modelling or Grey Box modelling

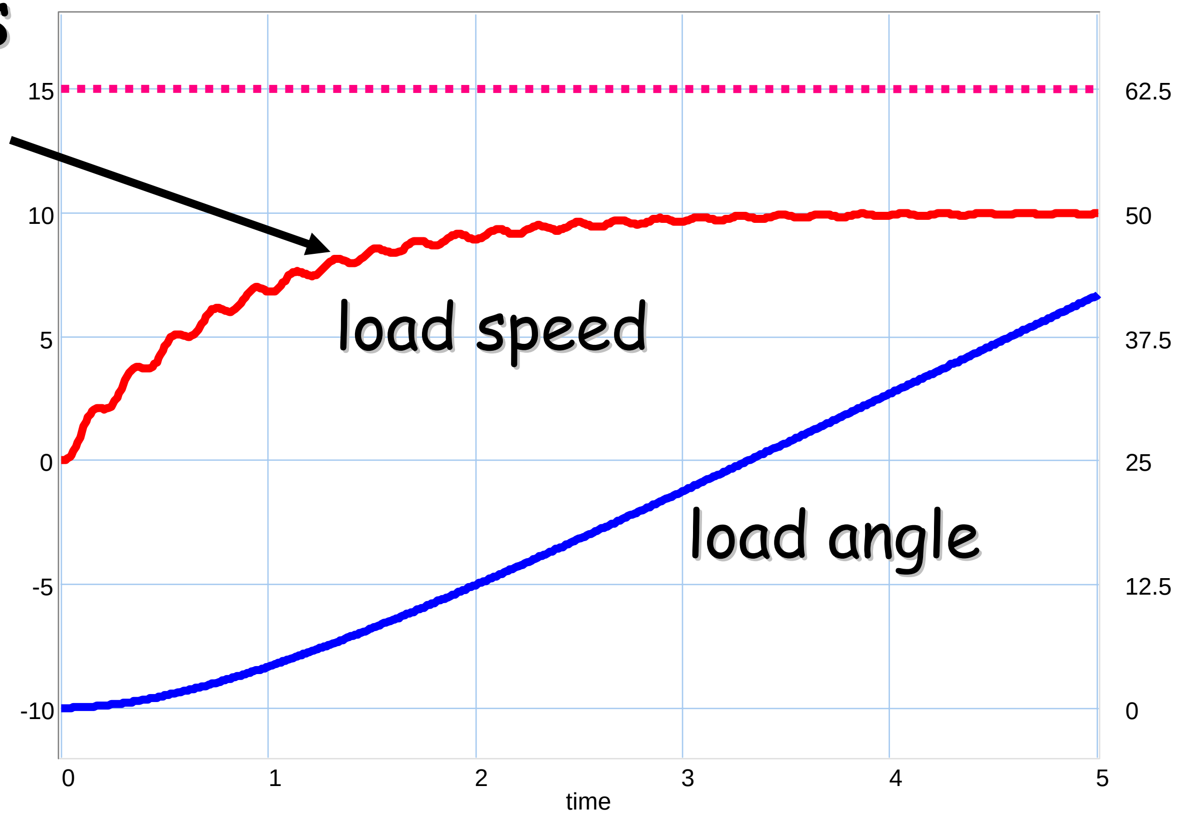
Bode plot


Magnitude (dB)
100
0
-100
-200
-300
$\omega_{resonance} \approx$ 30 rad/s
0.01
0.1
1
10
100
1000
10000
Frequency (rad/sec)
Phase (deg)
0
-100
-200
-300
-400
-500
0.01
0.1
1
10
100
1000
10000
Frequency (rad/sec)

Example of lecture 2

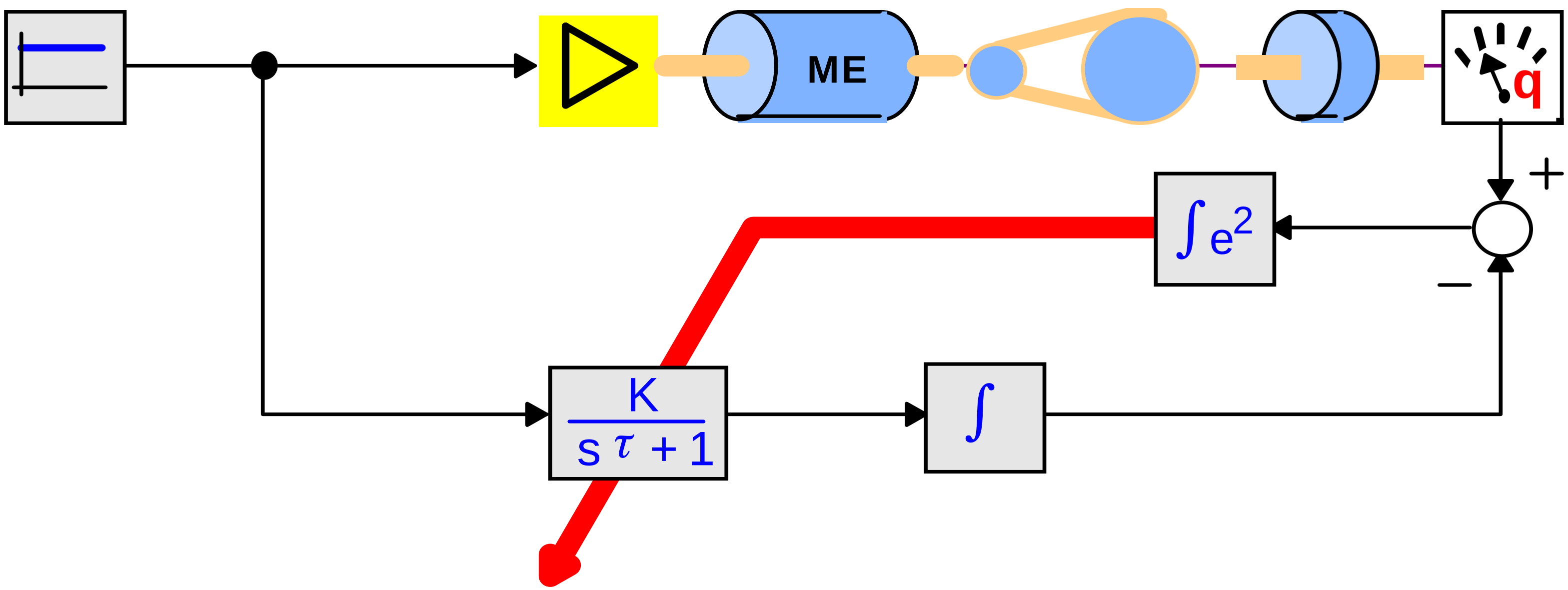
$T_{resonance} \approx 0.2$ s

$\omega_{resonance} \approx 30$



Response of load angle suggests poles in 0 and -a

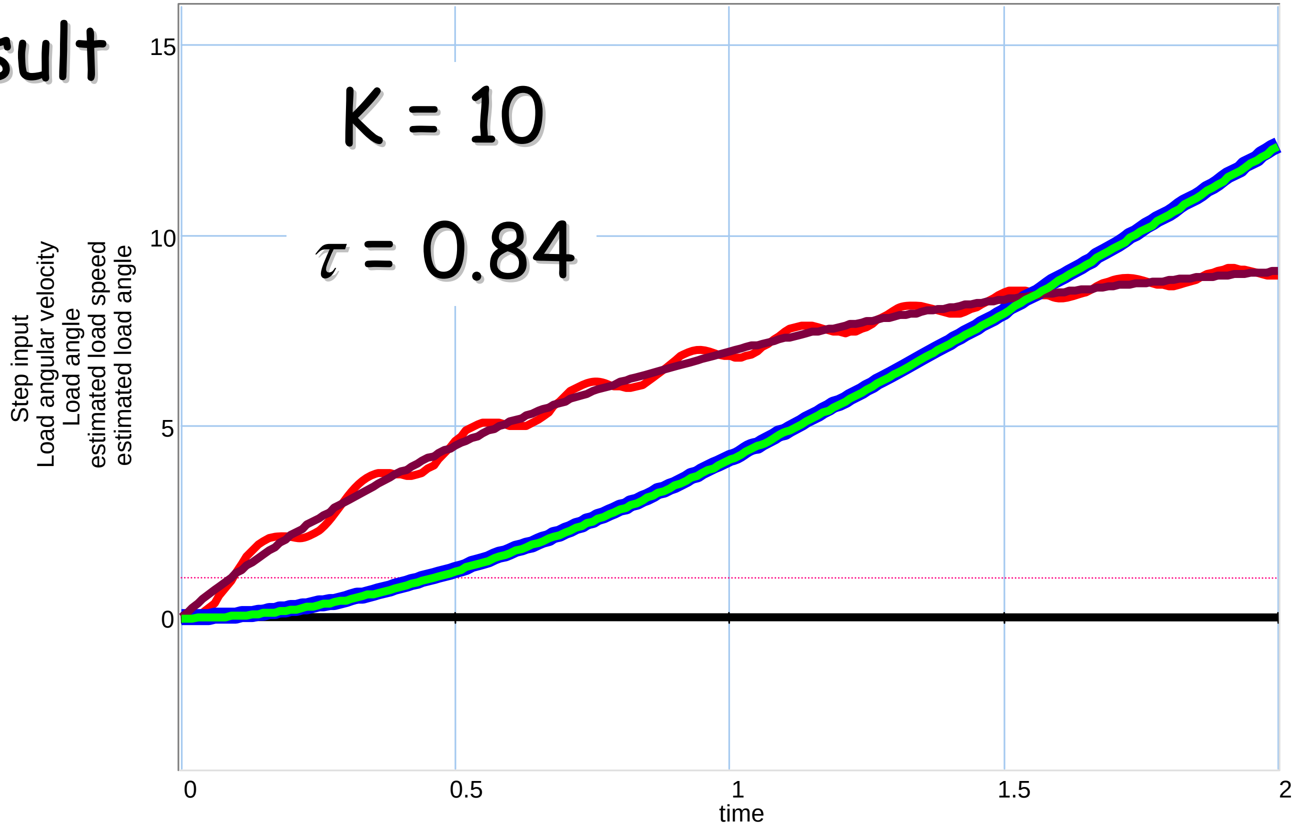
Identification experiment



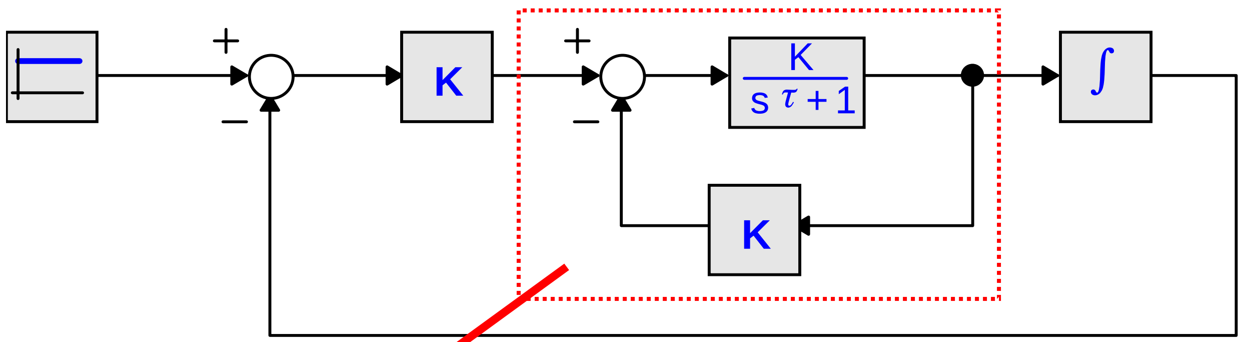
A1_Model_for_(exp)_identification.em

Identification experiment

Result



Proposed control structure



$$\frac{K'}{s+a+K'K_d}$$

$$\frac{K'K_p}{s\left(s+a+K'K_d\right)+K'K_p}$$

$$-\frac{1}{K_d}=\frac{K's}{s\left(s+a\right)+K'K_p}$$

$$-\frac{1}{K_p}=\frac{K'}{s\left(s+a\right)}$$

Root locus K_p

$$-\frac{1}{K_p} = \frac{K'}{s(s+a)}$$

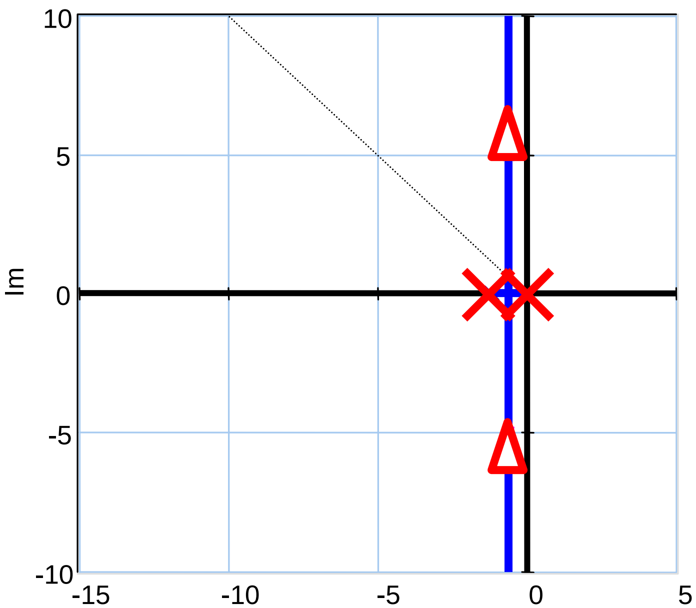
$a = -1.2$

$K' = 10 \cdot 1.2 = 12$

Stay away from the resonance frequency (30 rad/s):

e.g. $\omega_n = 6$ rad/s

$K_p \approx 36/12 = 3$



Design goal based on mechanical limitations

Root locus K_d

$$-\frac{1}{K_d} = \frac{K's}{s(s+a)+K'K_p}$$

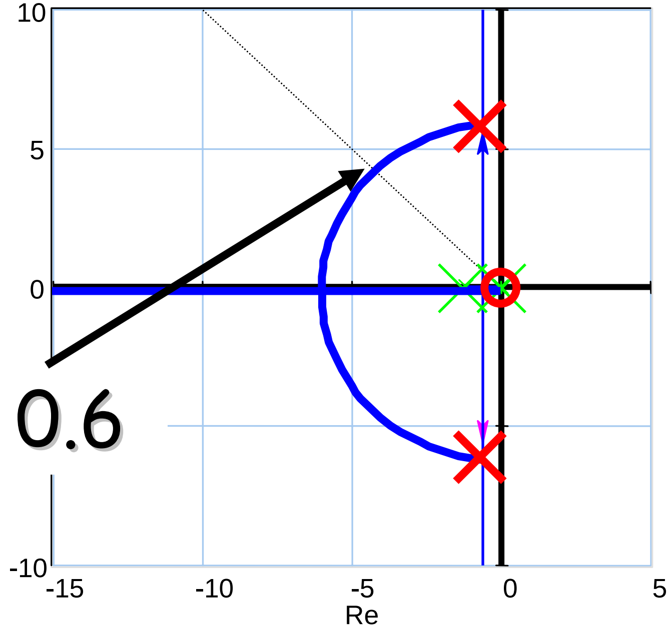
$$-\frac{1}{K_d} = \frac{12s}{s(s+a)+36}$$

In a similar way we can find for K_p = 4

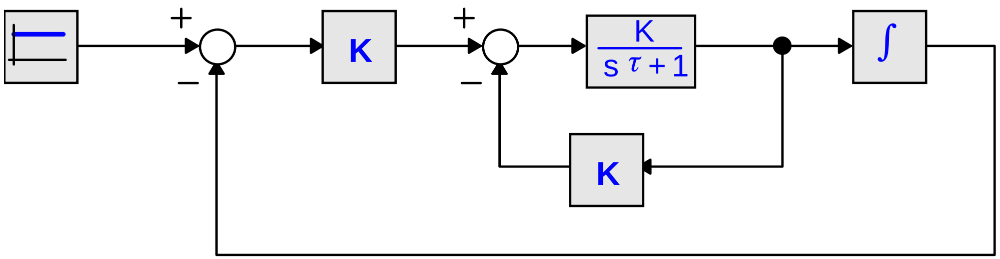
K_d = 0.8

(ω_n = 7 rad/s)

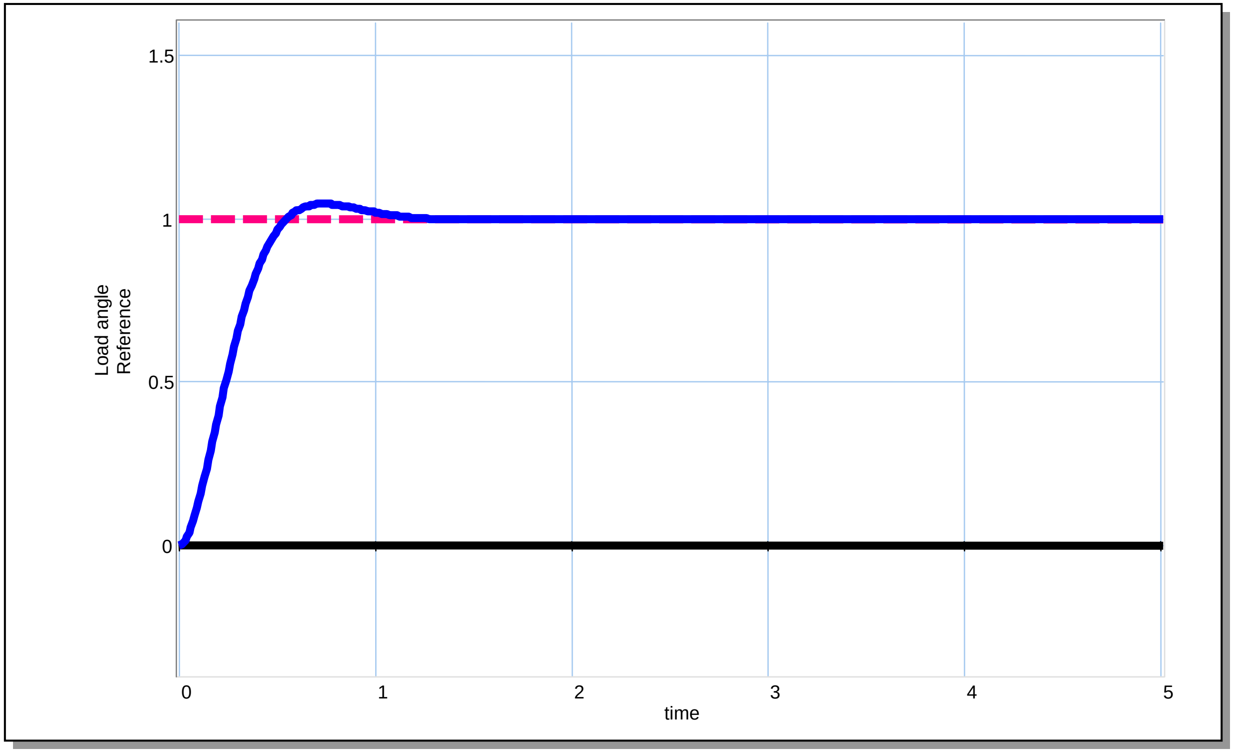
$K_d \approx 0.6$



Response of ‘ideal’ system



$K_p = 3$
$K_d = 0.6$



A2_Prop_plus_tacho_FB_exp_model.em

Alternative design

- Use state space representation and select ω_n (factor 5 smaller than resonance frequency) and desired z

$$A' = \begin{pmatrix} 0 & 1 \\ -K'K_p & -a-K'K_d \end{pmatrix} = \begin{pmatrix} 0 & 1 \\ -\omega_n^2 & -2z\omega_n \end{pmatrix}$$

$$A' = \begin{pmatrix} 0 & 1 \\ -12K_p & -1.2-12K_d \end{pmatrix} = \begin{pmatrix} 0 & 1 \\ -36 & -8.4 \end{pmatrix}$$

$$K_p = 3$$

$$K_d = 0.6$$

In “real” system

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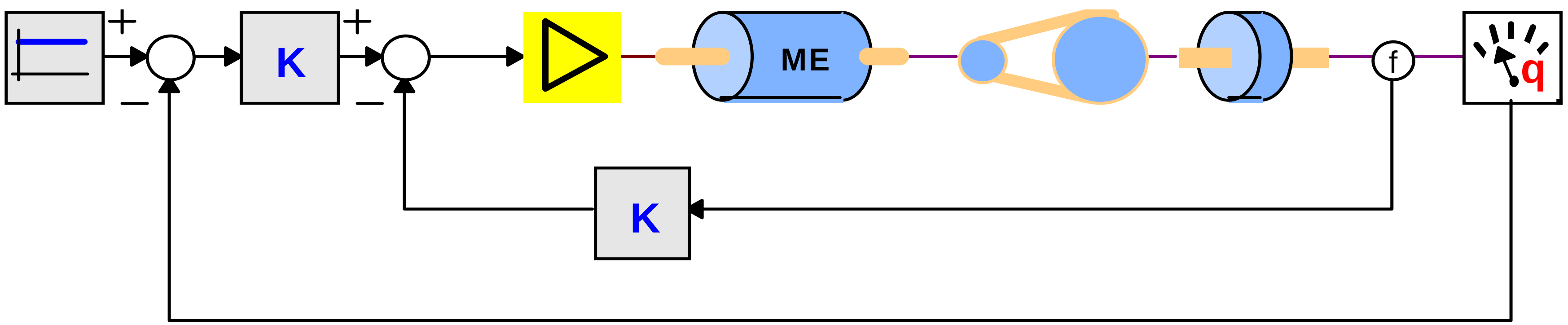

A3_Prop_plus_tacho_FB_real_model.em

Response of ‘real’ system

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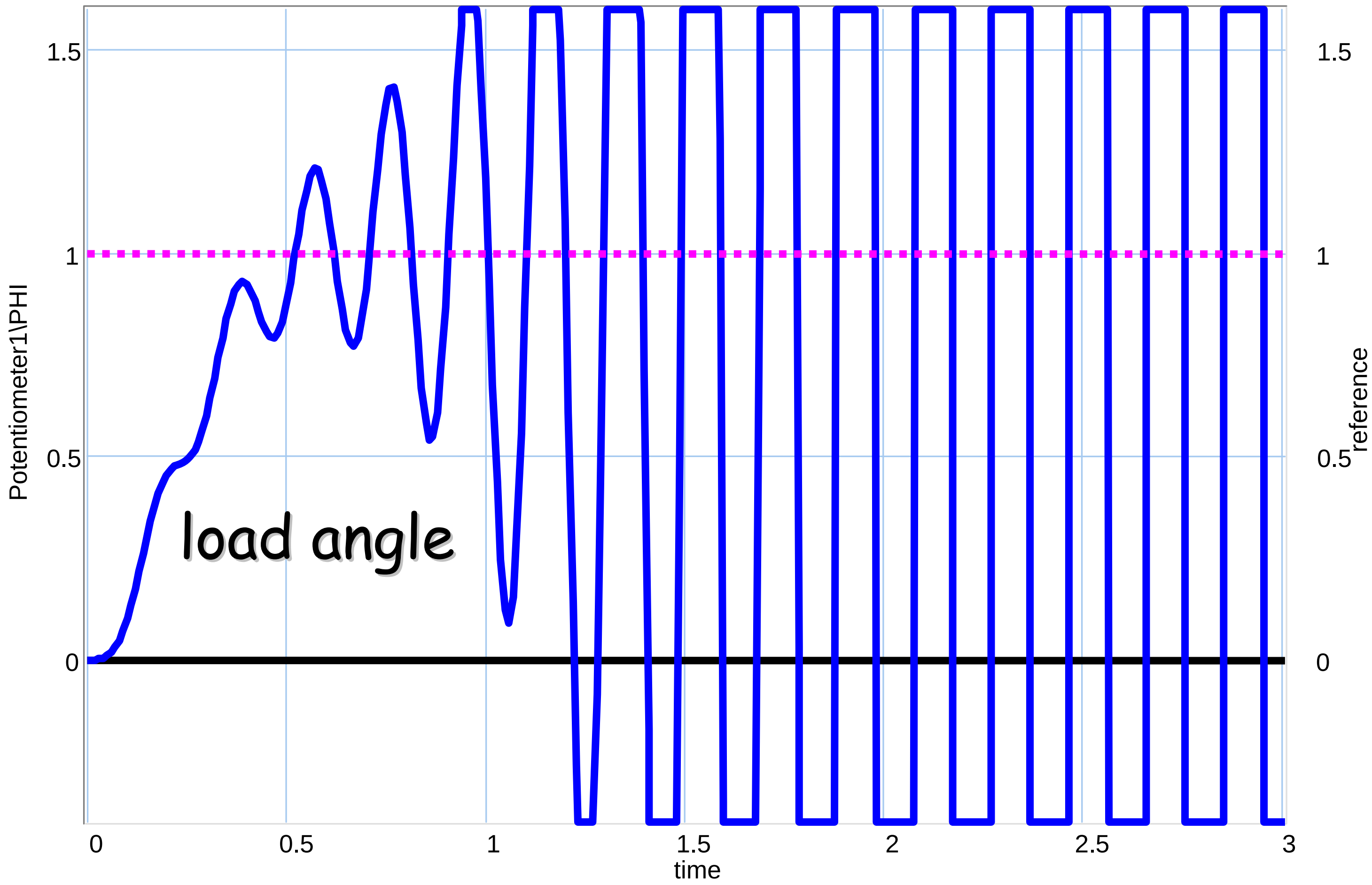
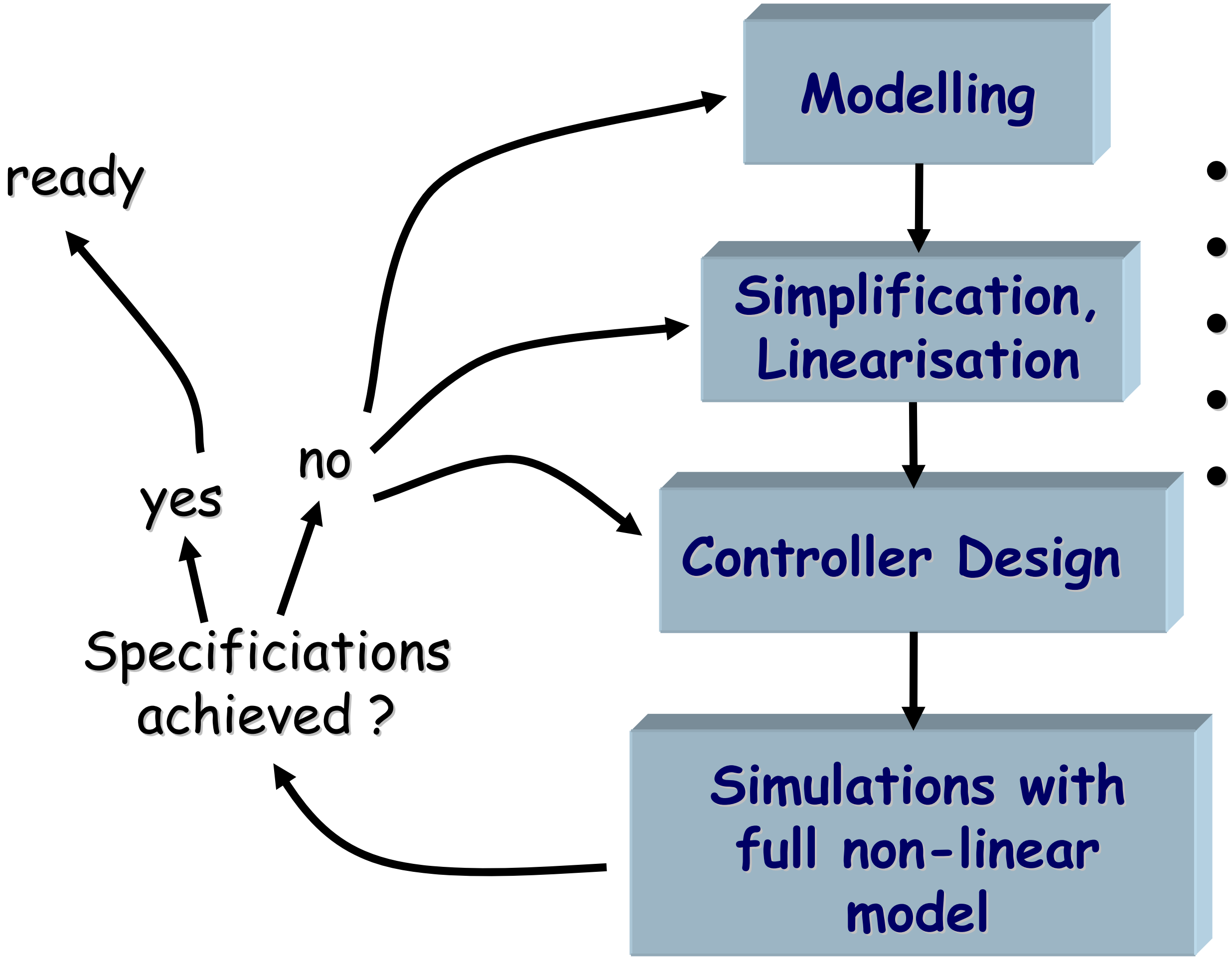


Design issues (from lecture 1)



- speed of response
- bandwidth
- stability
- overshoot
- sensitivity for disturbances and parameter variatons

Tacho feedback in “real” system

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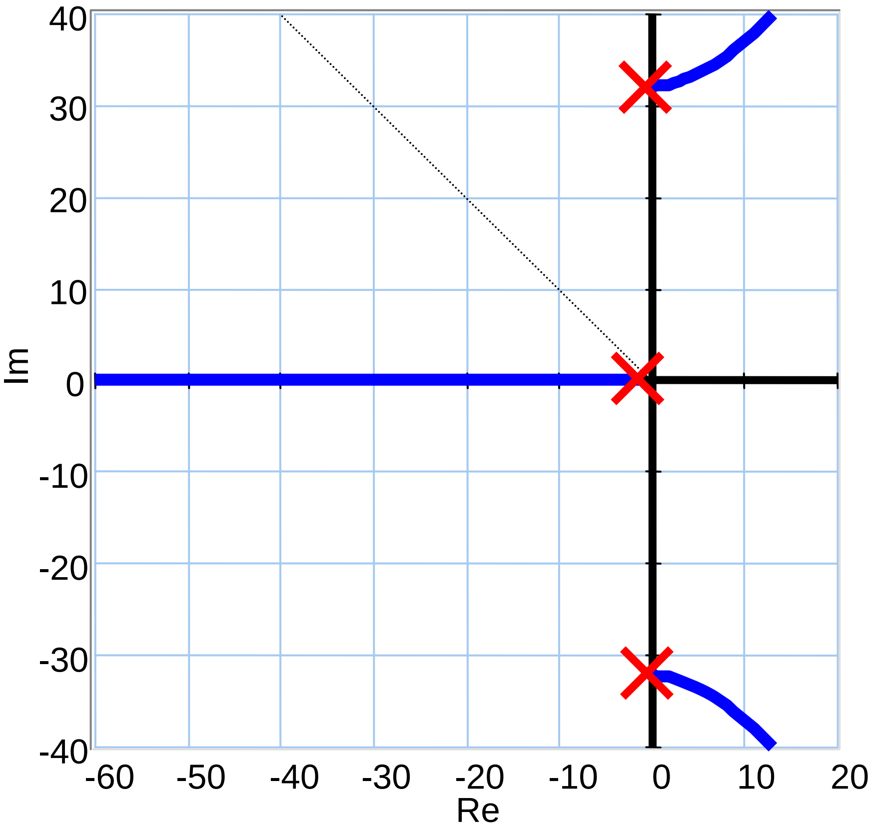
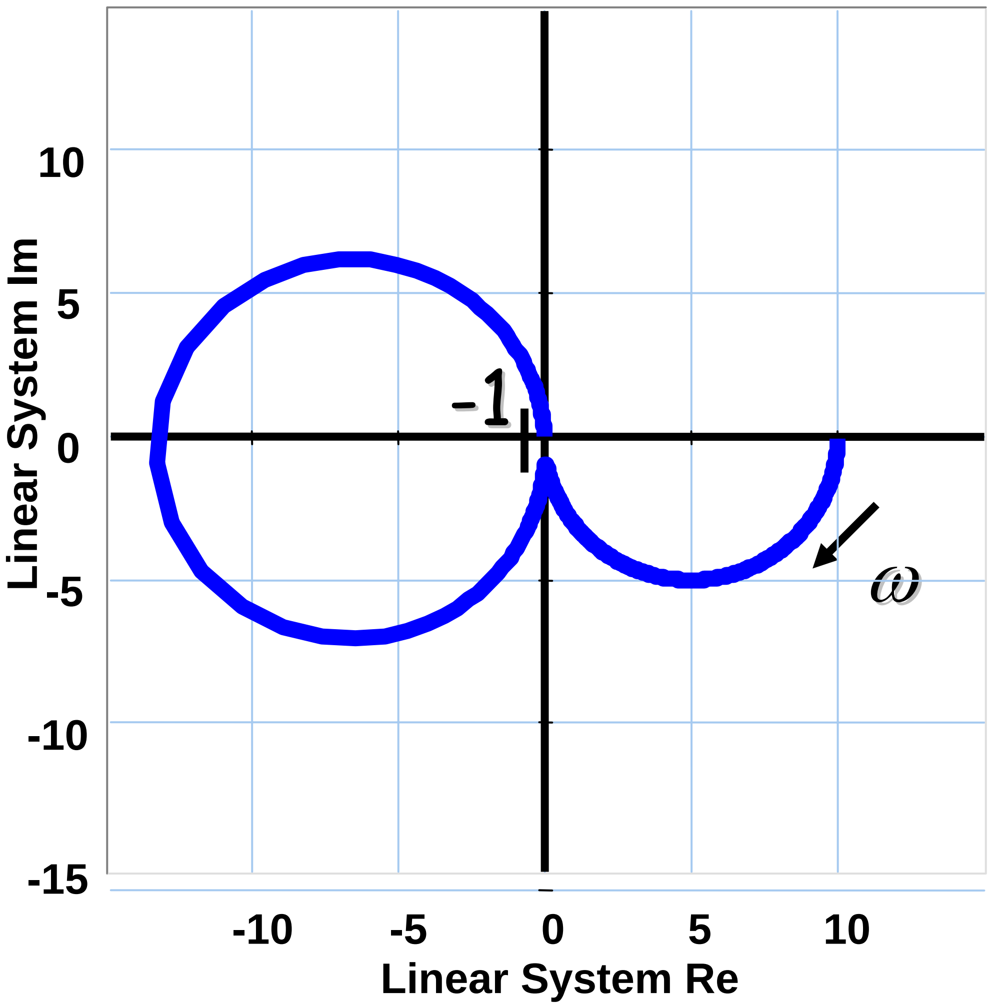
A_Model_for_identification.em

(tacho -feedback)

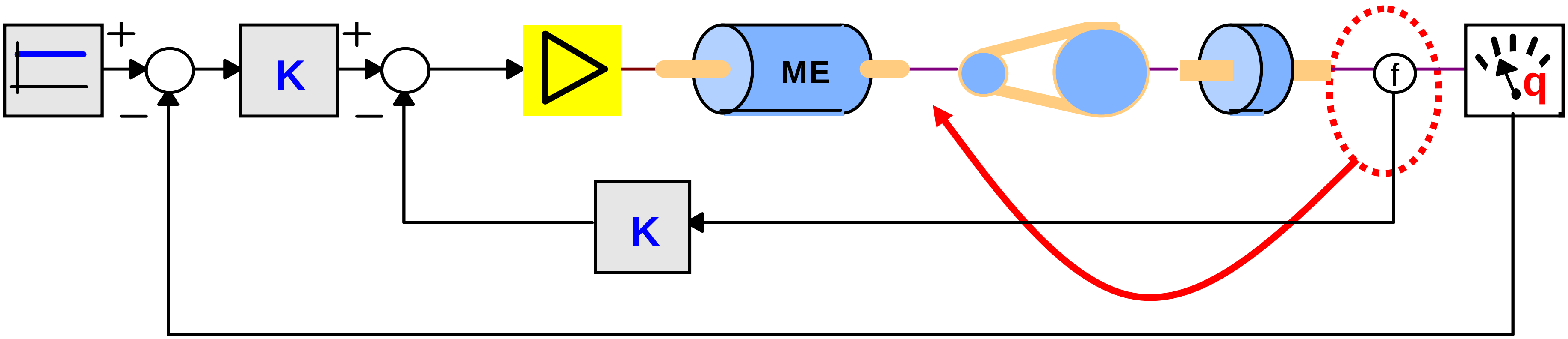
Due to (disregarded) complex poles, tacho feedback of no use here



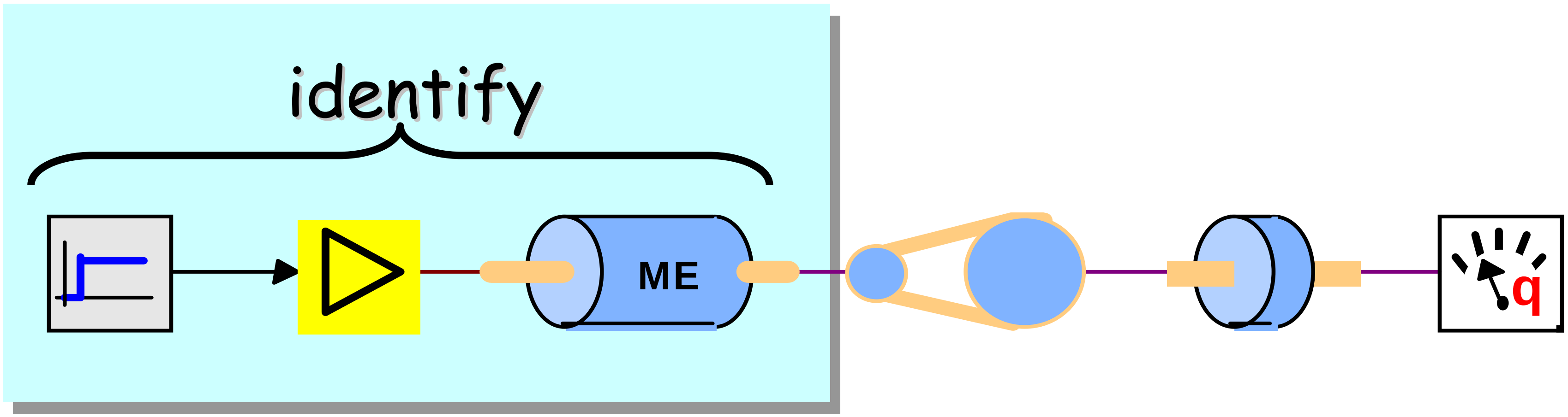
Nyquist



Alternative tacho feedback



New linearisation



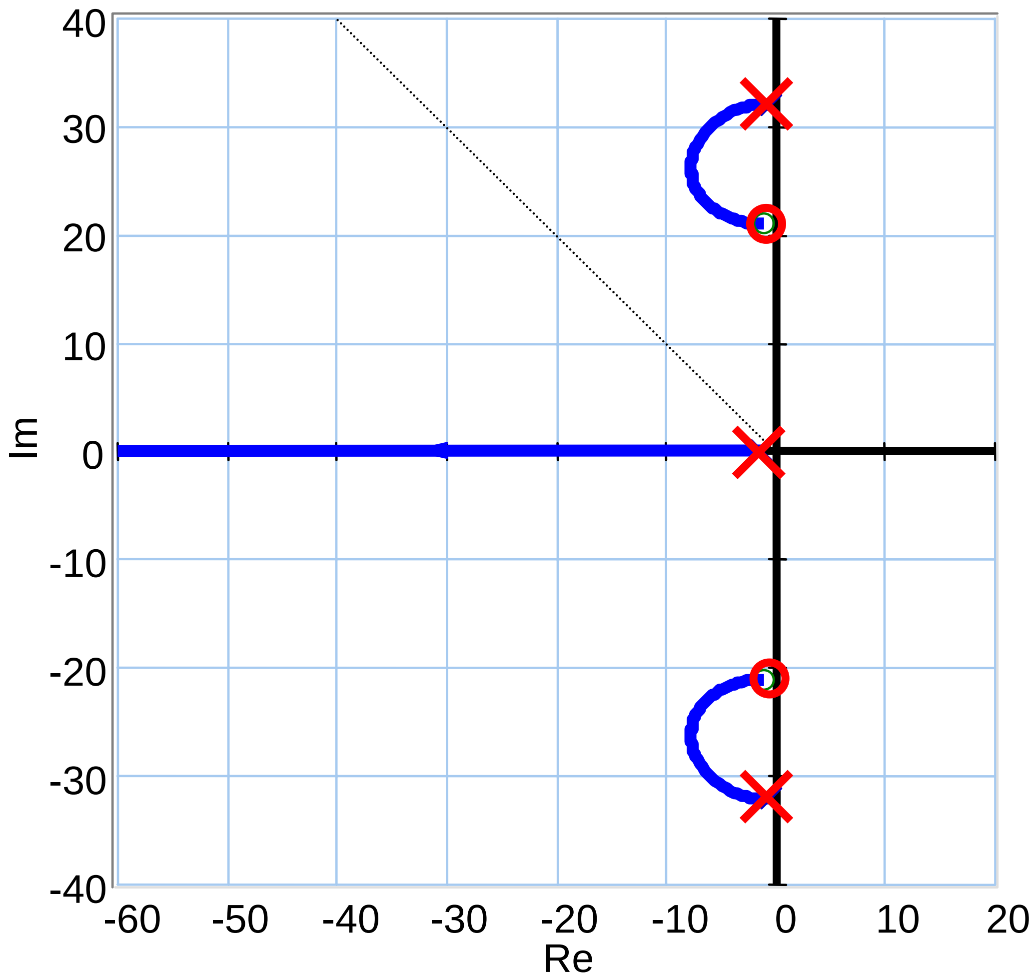
A_Model_for_identification.em

This helps !

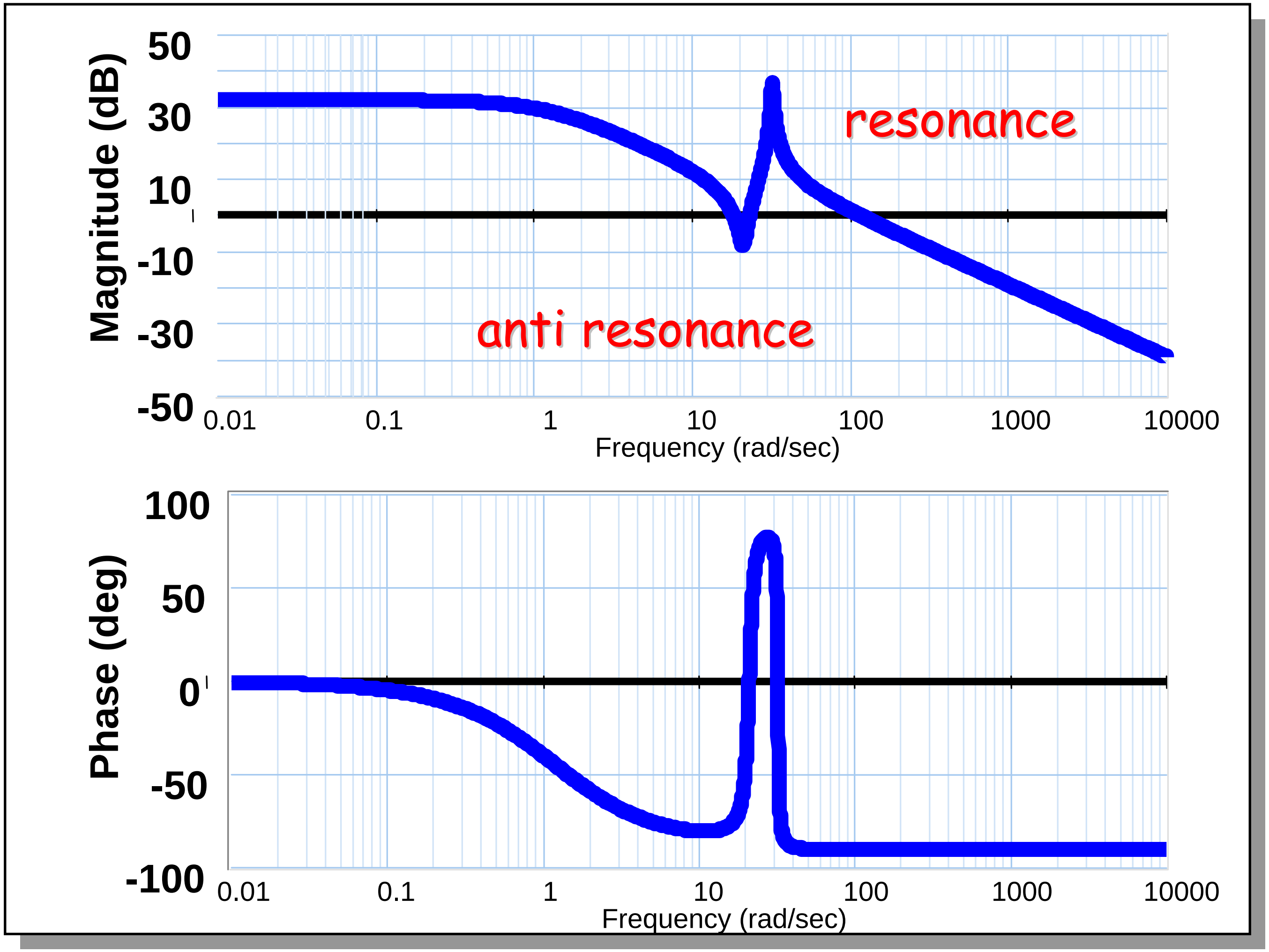
Complex poles now compensated by complex zeros

On real axis tacho feedback does what it is expected to do !

collocated control



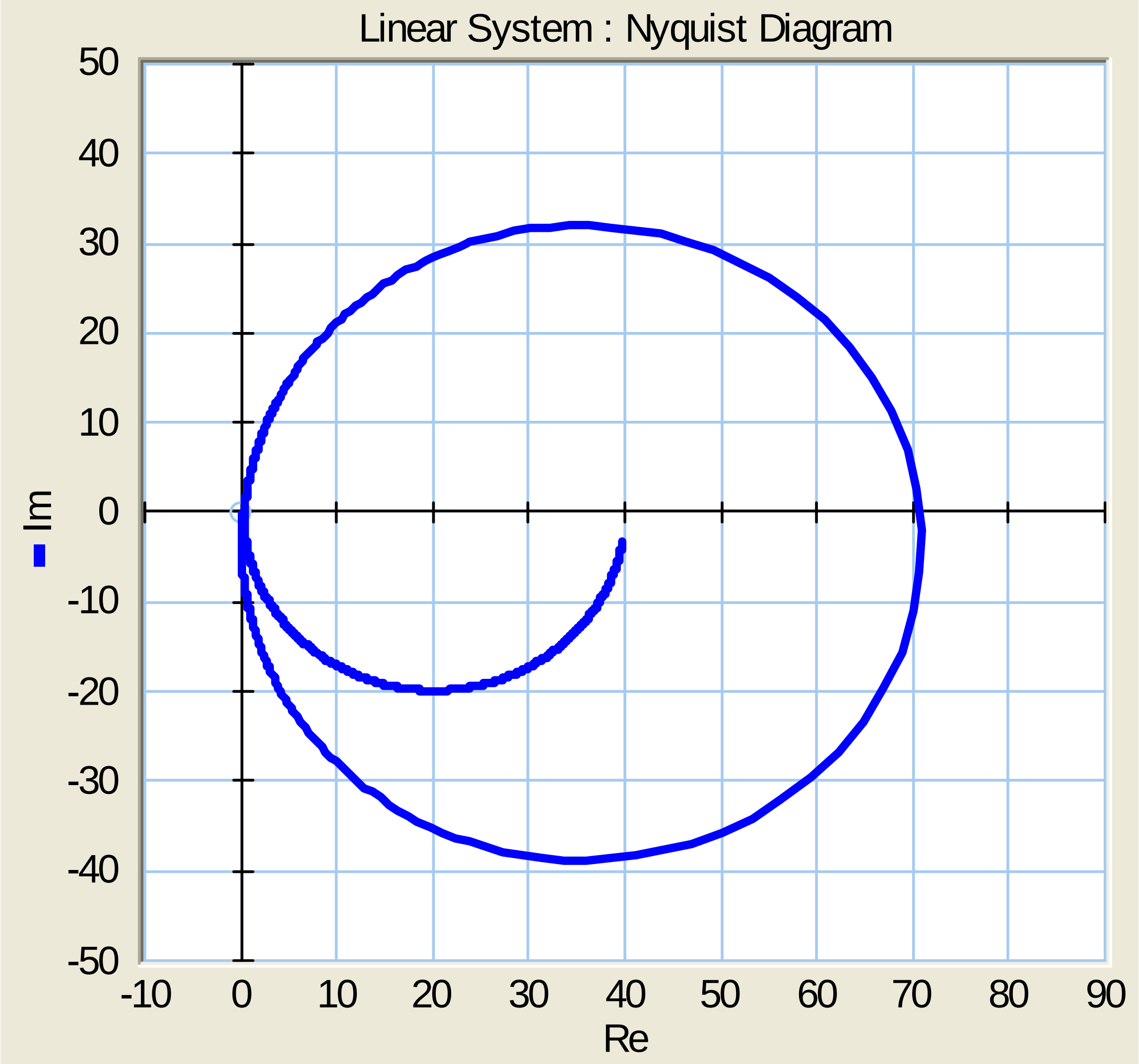
Bode


Magnitude (dB)
50
30
10
-10
-30
-50
0.01
0.1
1
10
100
1000
10000
Frequency (rad/sec)
resonance
anti resonance
Phase (deg)
100
50
0
-50
-100
0.01
0.1
1
10
100
1000
10000
Frequency (rad/sec)

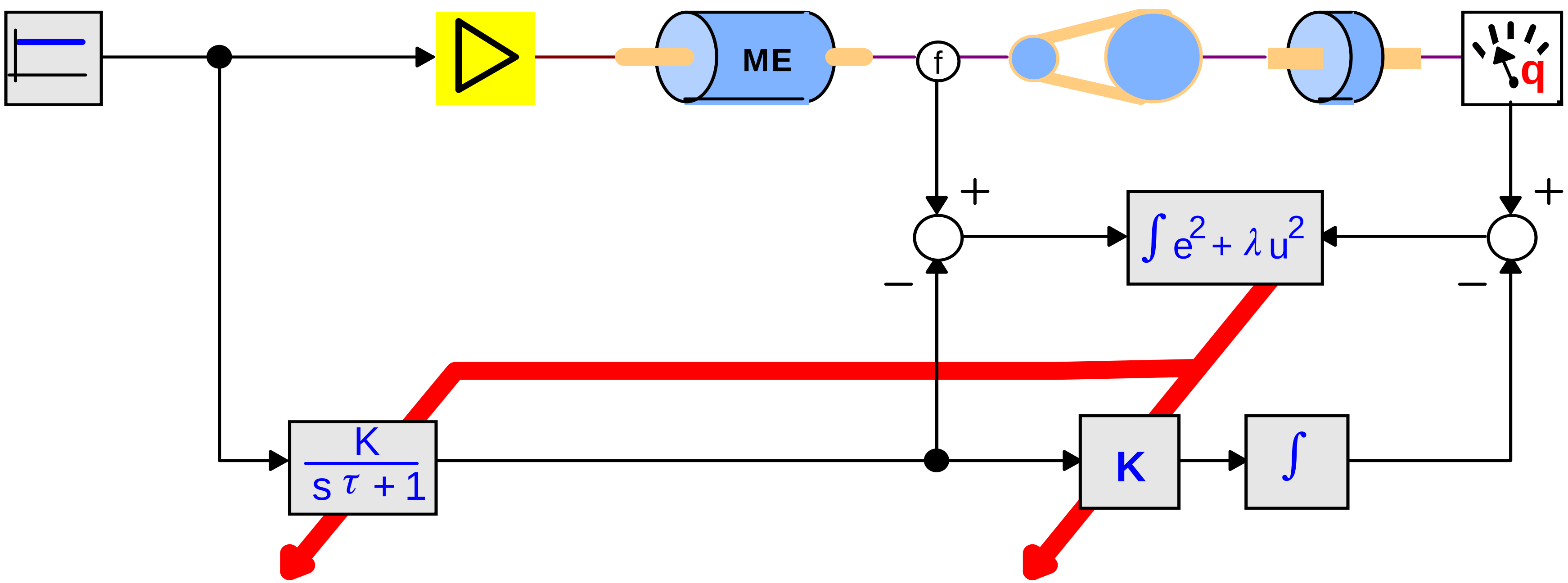
Nyquist

Passivitiy:
system behaves as a first-order system

Phase between +90 and -90 deg.

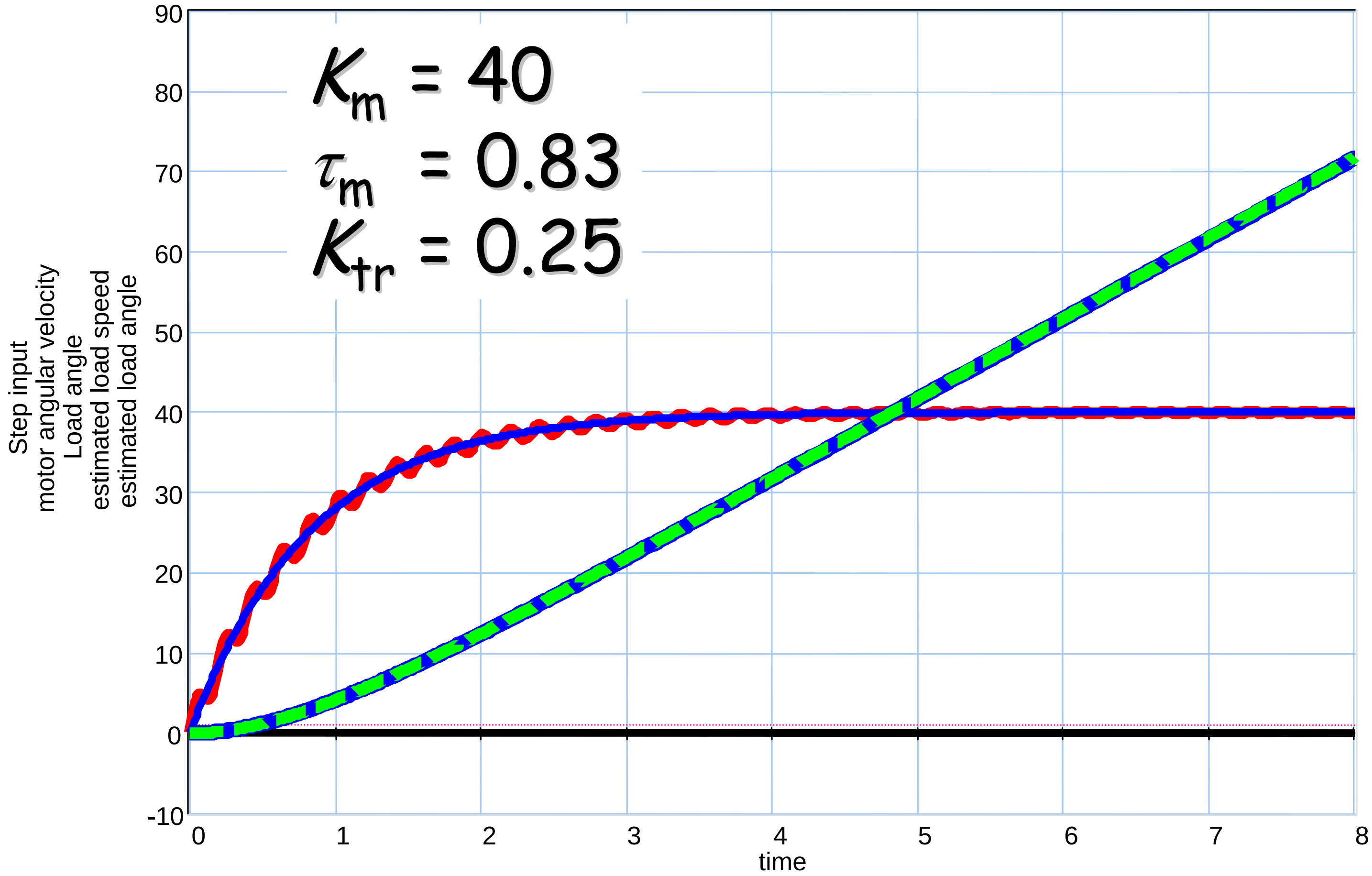


Experiment



A4_Model_for_(exp)_identification_motor_tacho_FB.em

Identification result



Redesign of controller

We found before:

$K_p = 3$
$K_d = 0.6$

or

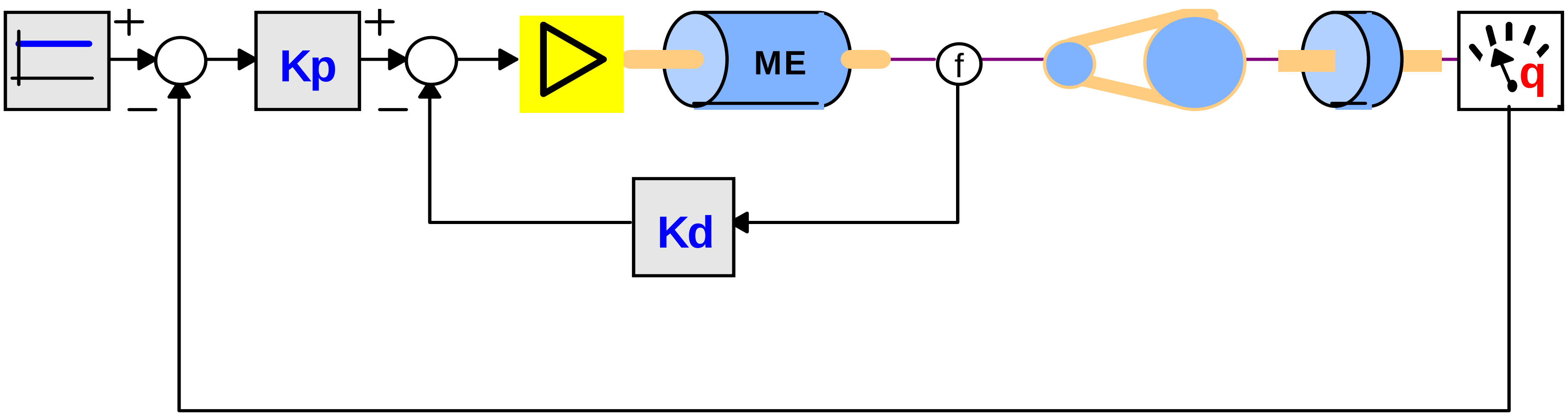
$K_p = 4$
$K_d = 0.8$

Because gain from input to motor is 4 times higher,

$K_{d,m} = 0.6/4 = 0.15$ (0.2)

$K_p = 3$ (4)

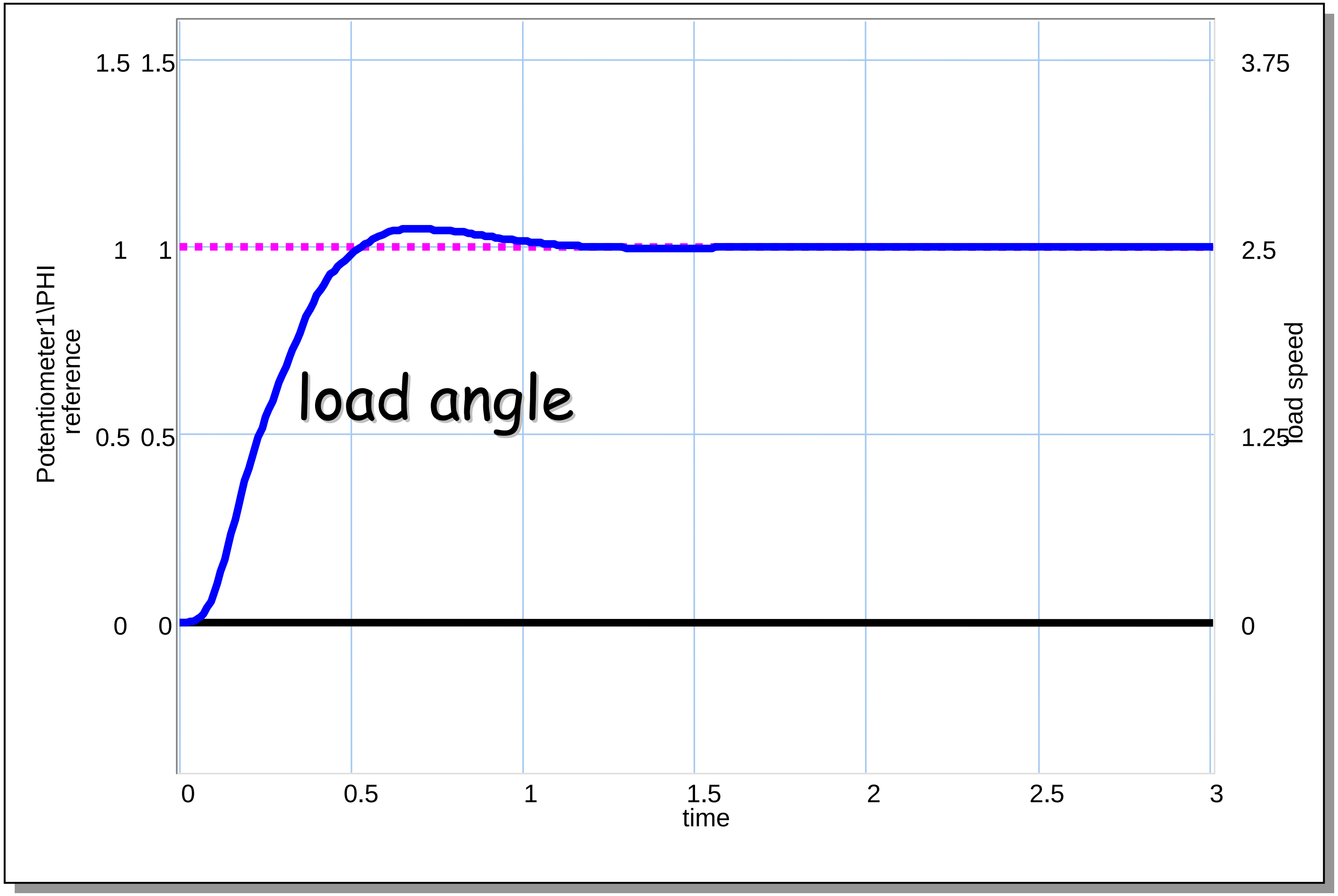
Result in 'real' system



C_Prop_plus_Tacho_feedback.em

Stepresponse

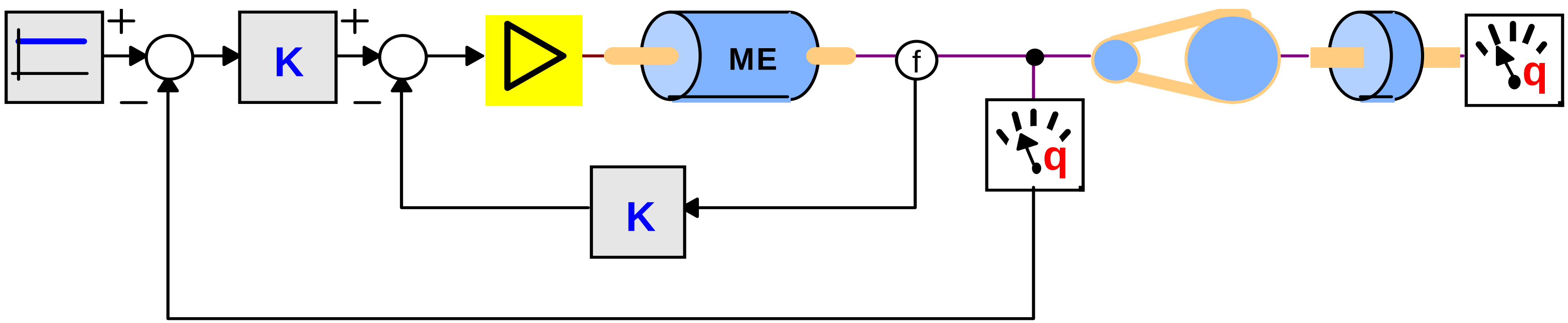
$K_p = 3$
$K_d = 0.6/4$
$= 0.15$



Tacho feedback

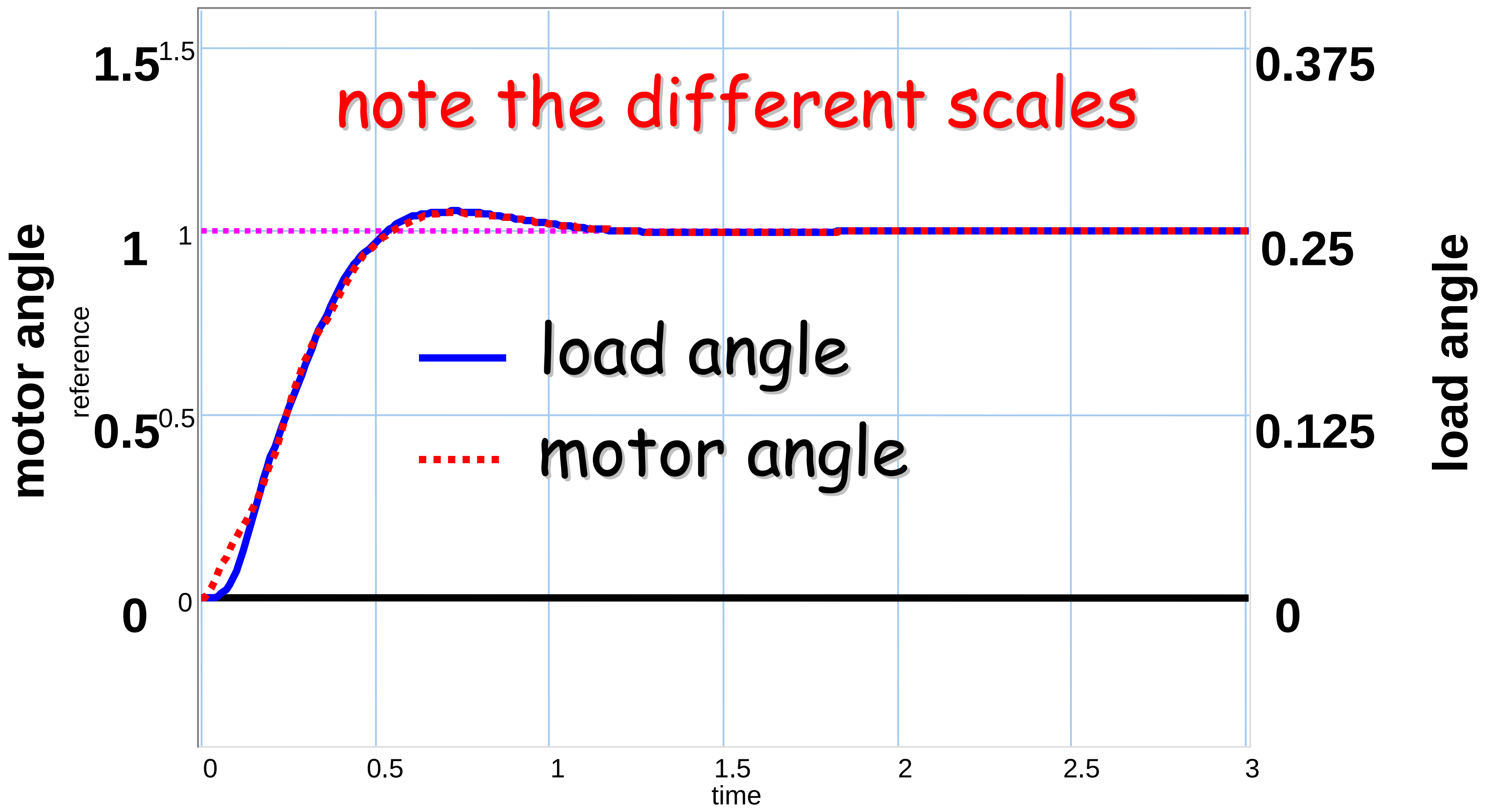
- Tacho feedback should always be based on the motor speed
- Tacho feedback of the load leads in a system with resonant poles easily to an unstable system

Motor feedback only

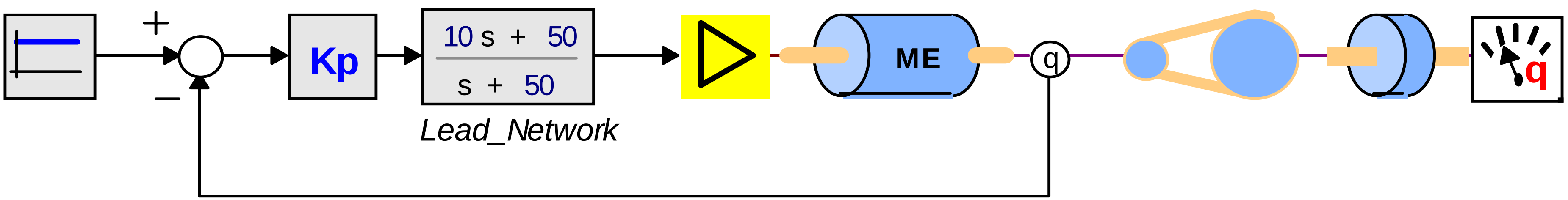


C1_Prop_plus_Tacho_feedback_motor_only.em

Responses

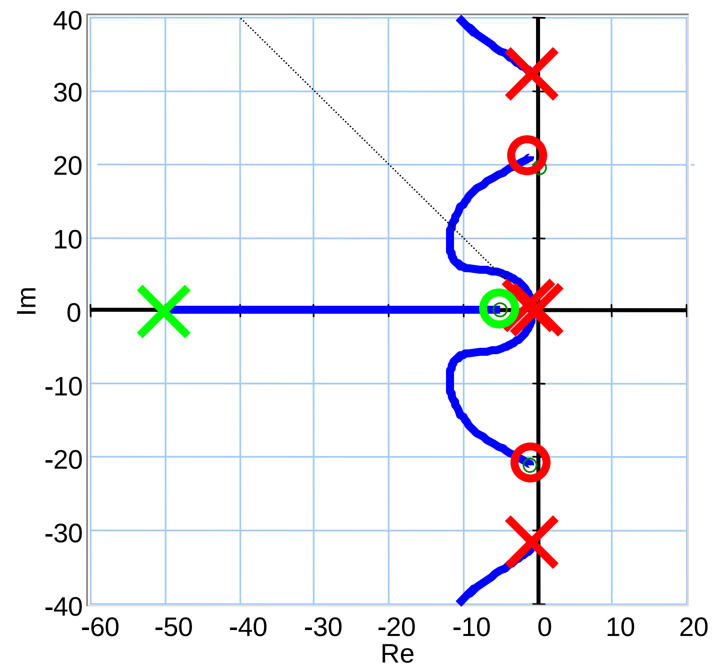

note the different scales
1.5
1.5
1
1
0.5
0.5
0
0
motor angle
reference
0.375
0.25
0.125
0
load angle
load angle
motor angle
0
0.5
1
1.5
2
2.5
3
time

Lead network



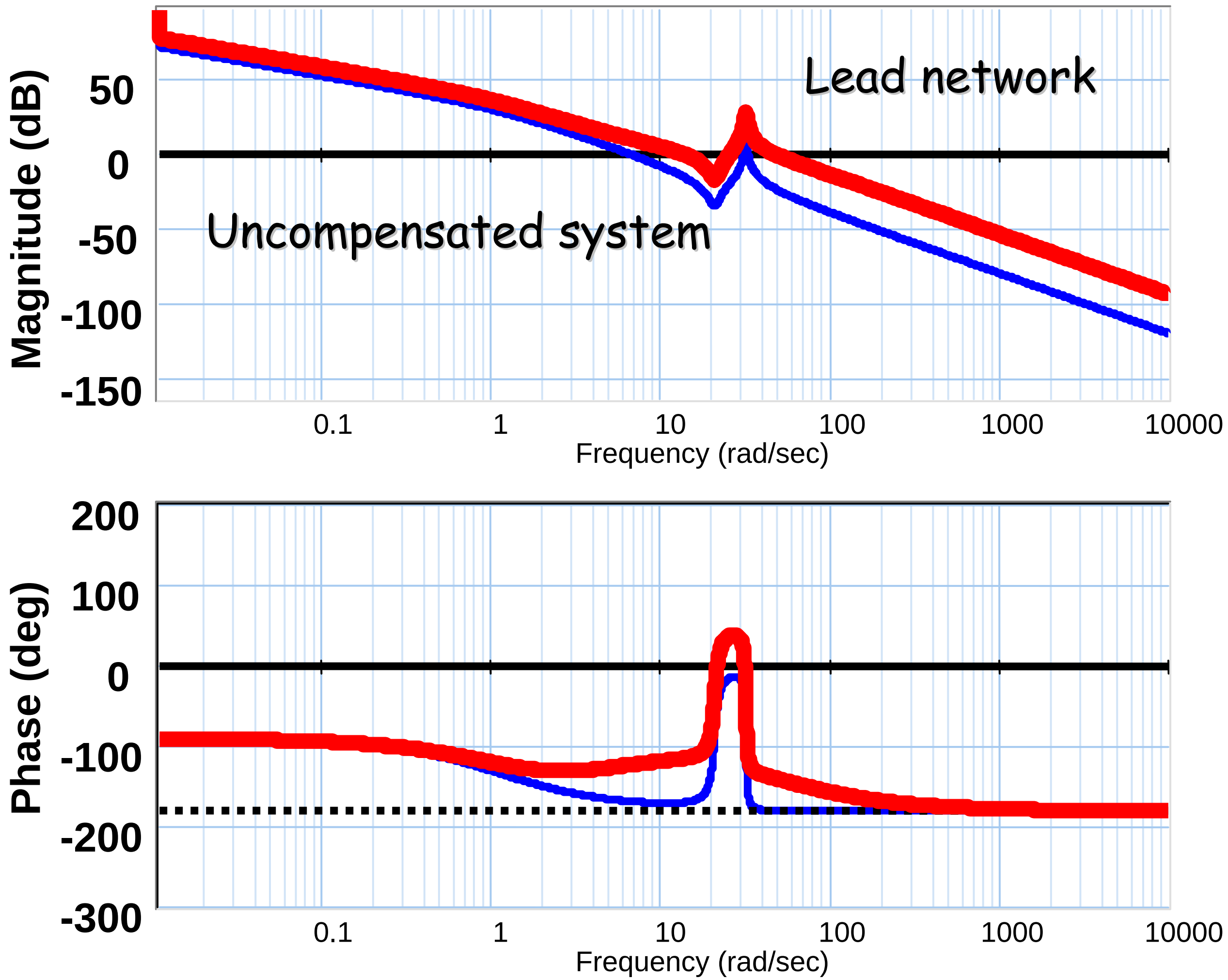
Lead network:

K = 1.9
zero in -5
pole in -50

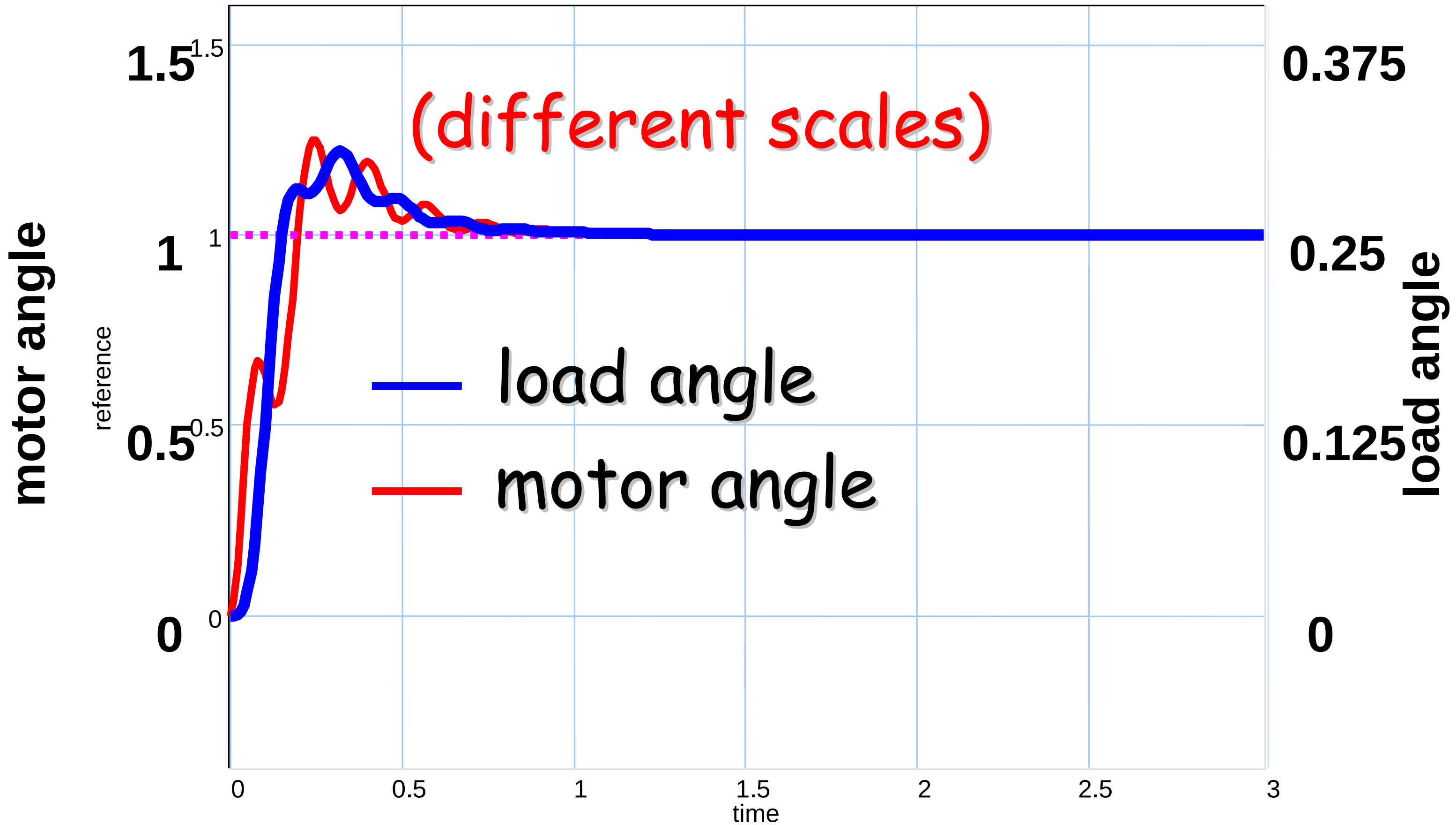


C2_lead_network_motor_only_no prefilter.em

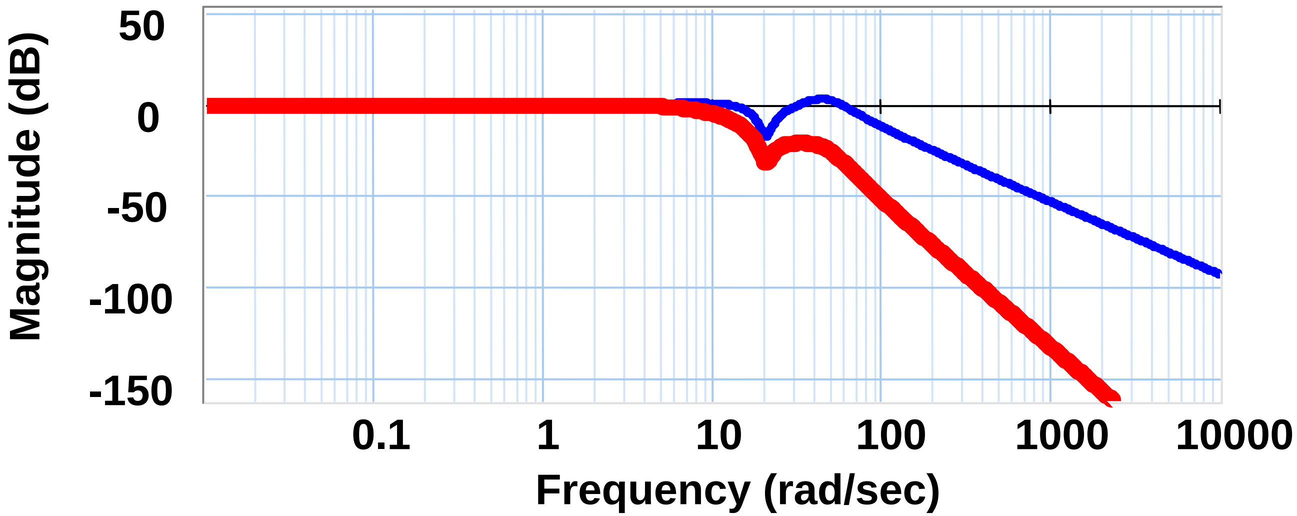
Bode


Magnitude (dB)
50
0
-50
-100
-150
Lead network
Uncompensated system
0.1
1
10
100
1000
10000
Frequency (rad/sec)
Phase (deg)
200
100
0
-100
-200
-300
0.1
1
10
100
1000
10000
Frequency (rad/sec)

Response

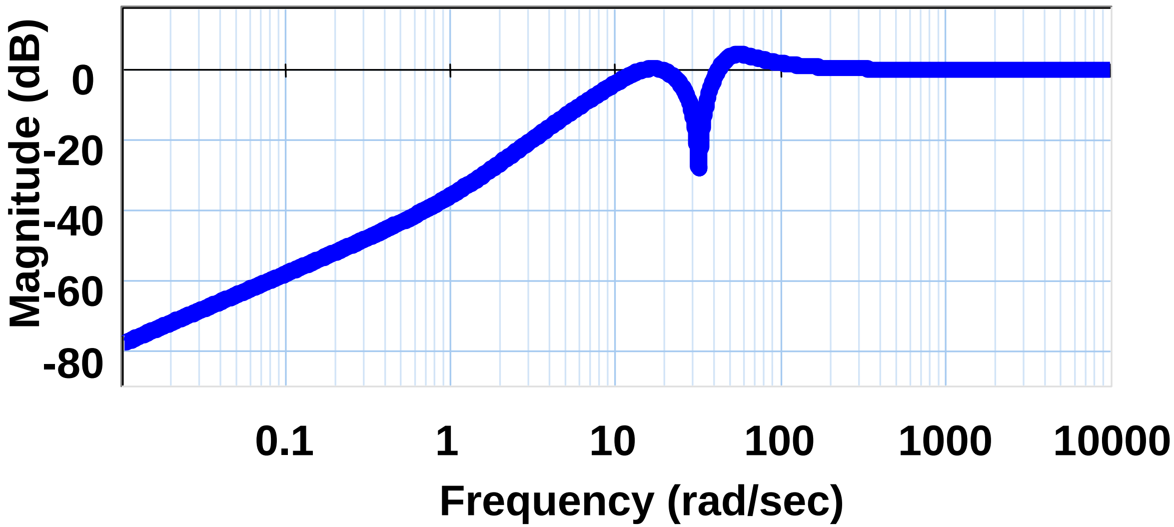

(different scales)
load angle
motor angle
motor angle
reference
load angle
1.5
1
0.5
0
0.375
0.25
0.125
0
time
0
0.5
1
1.5
2
2.5
3

Bode Closed-loop system



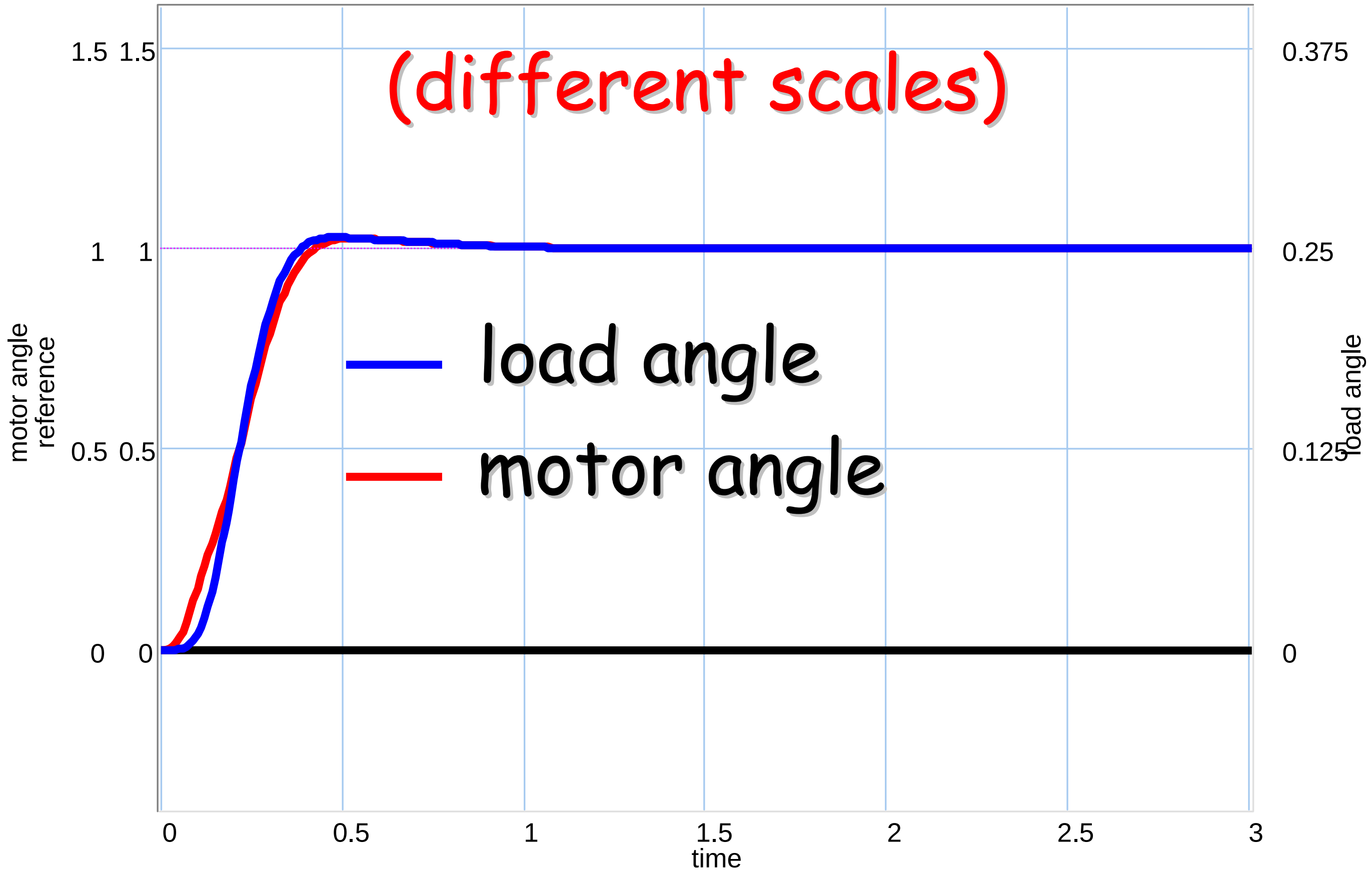
with prefilter in -10 ± 2j

Sensitivity

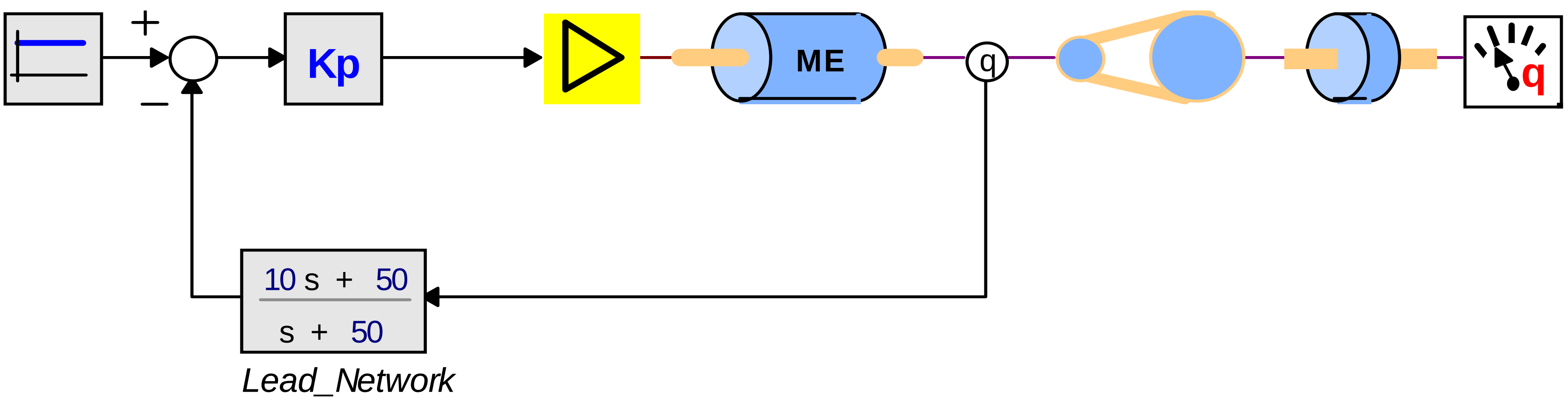


For disturbances
the resonance peak is
not suppressed

Response with prefilter



Lead network in feedback



C2_lead_network_in_FB_motor_only.em

Responses

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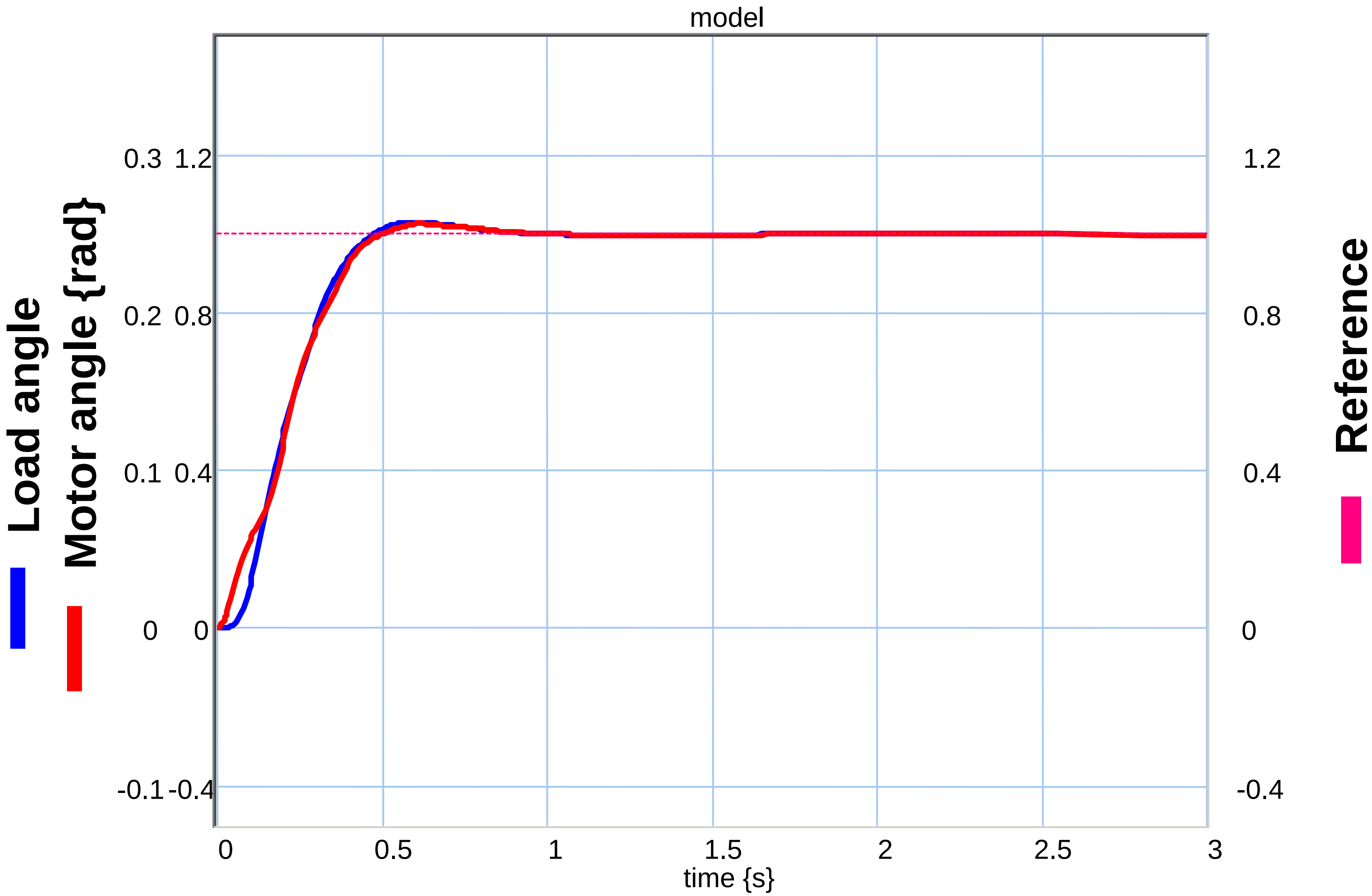

Motor angle feedback & derivative of motor angle

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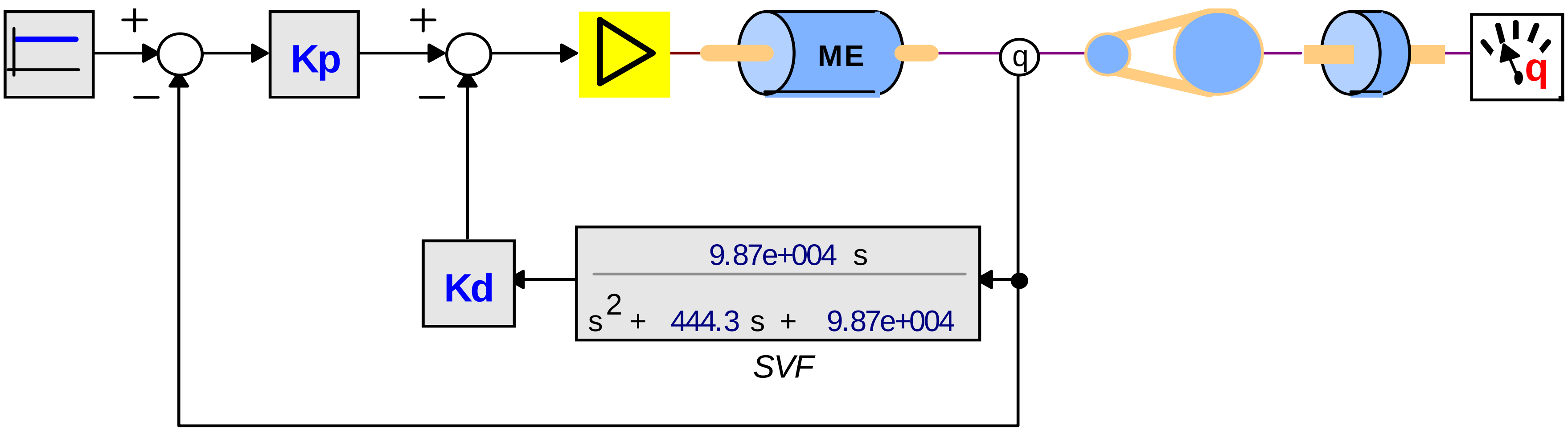

$$\text{SVF: } \frac{s\omega_n^2}{s^2 + 2\zeta\omega_n + \omega_n^2}$$

E1_fb_motor_only_SVF.em

$\omega_n =$ 10 times ω resonant poles

Responses

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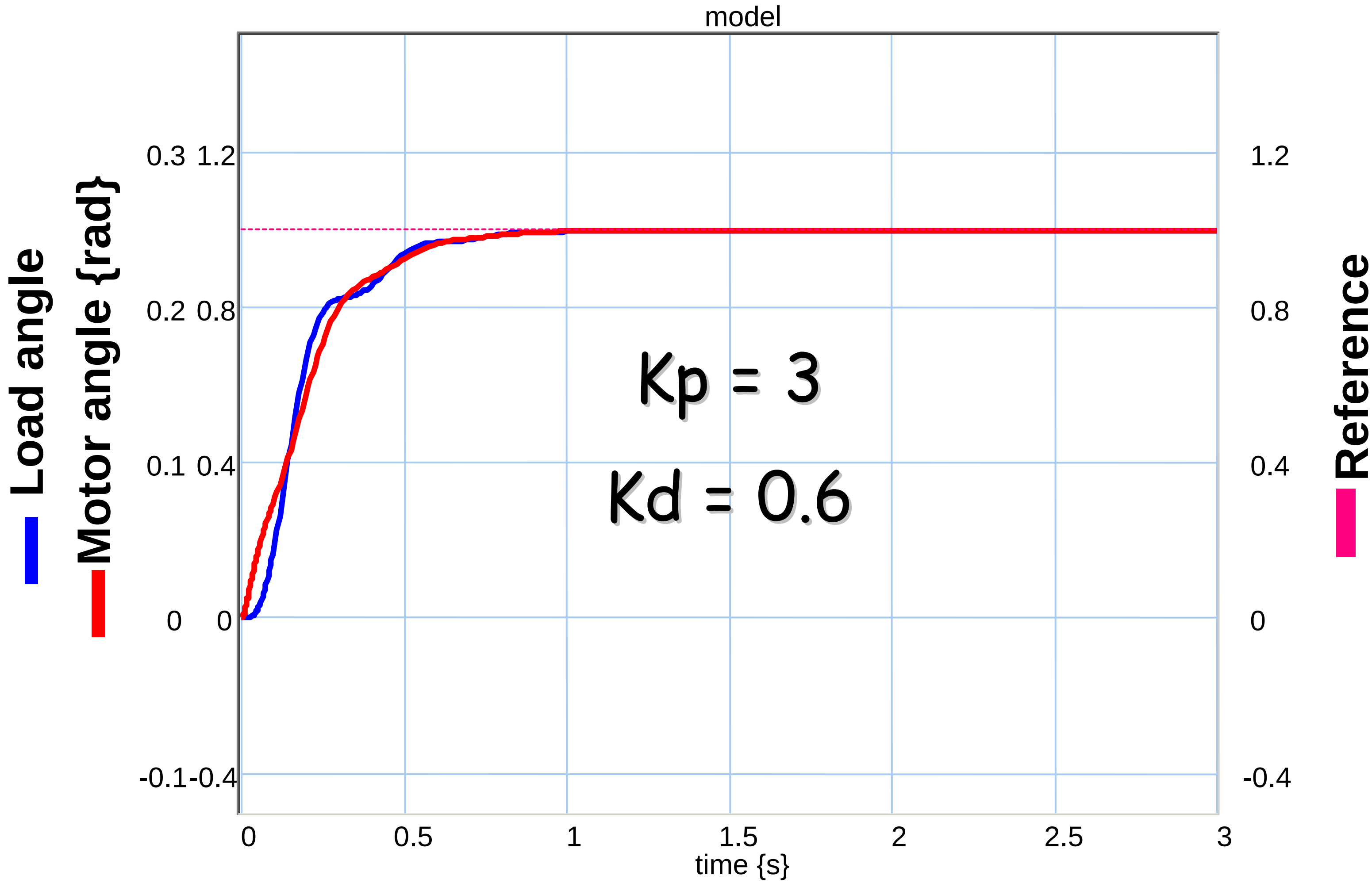

Further improvements

- Further improvements only possible by removing the limiting factor:
  - complex poles, due to limited stiffness of axis
  - a stiffer axis will move these poles to higher frequencies and
  - enable much better performance:
  - change k_{axis} from 1.45 into 100

Response with a stiffer axis

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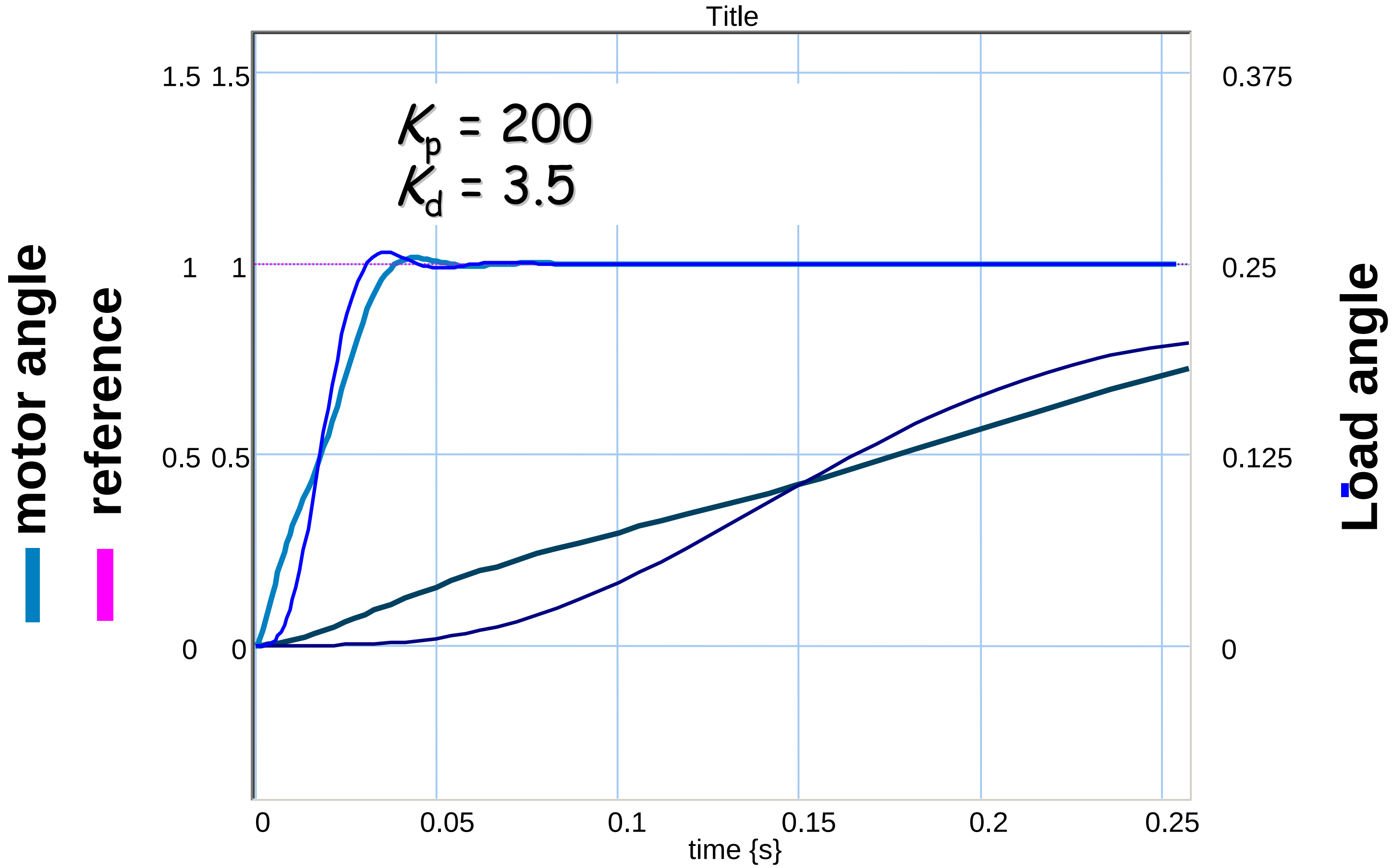
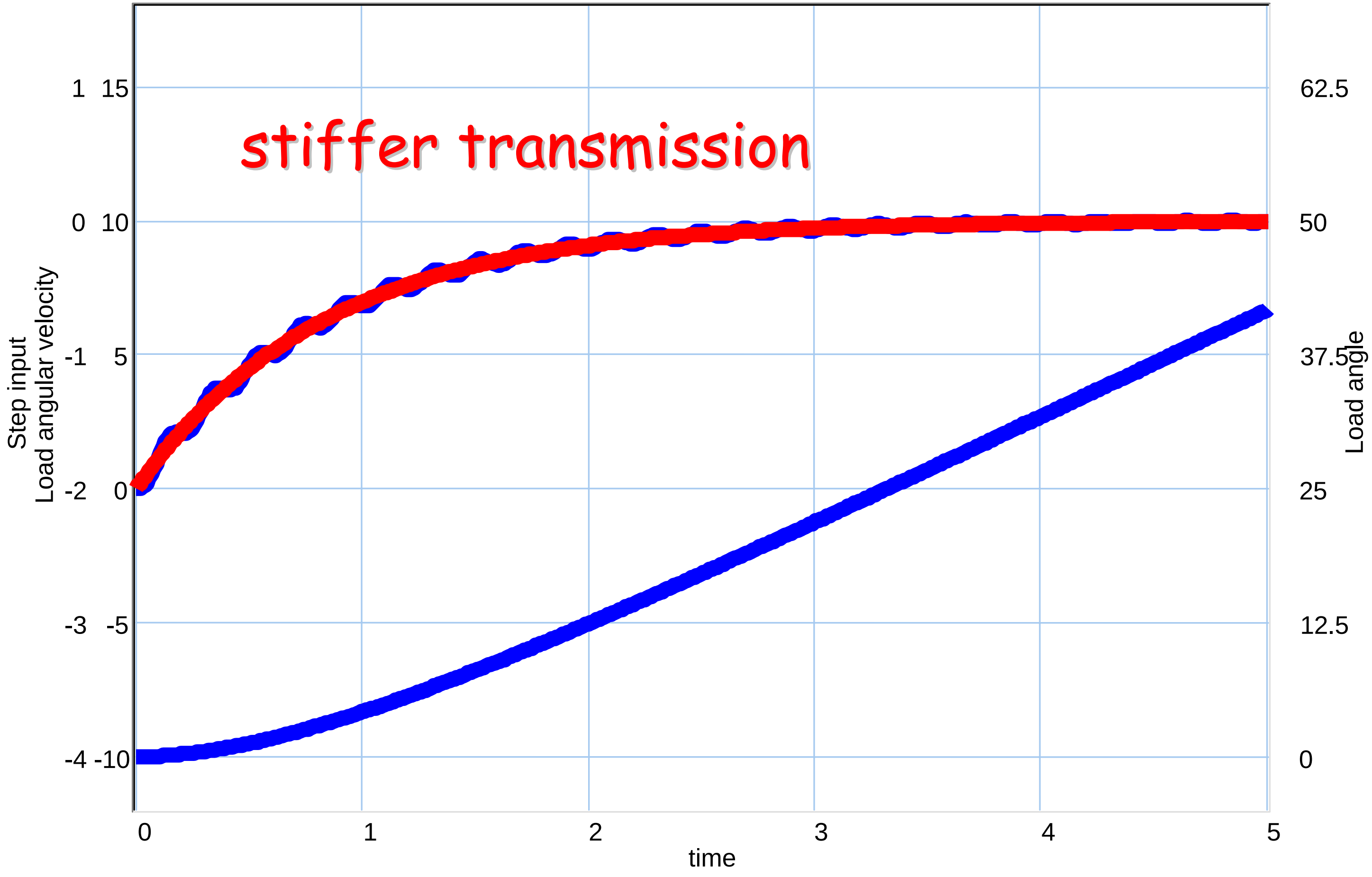
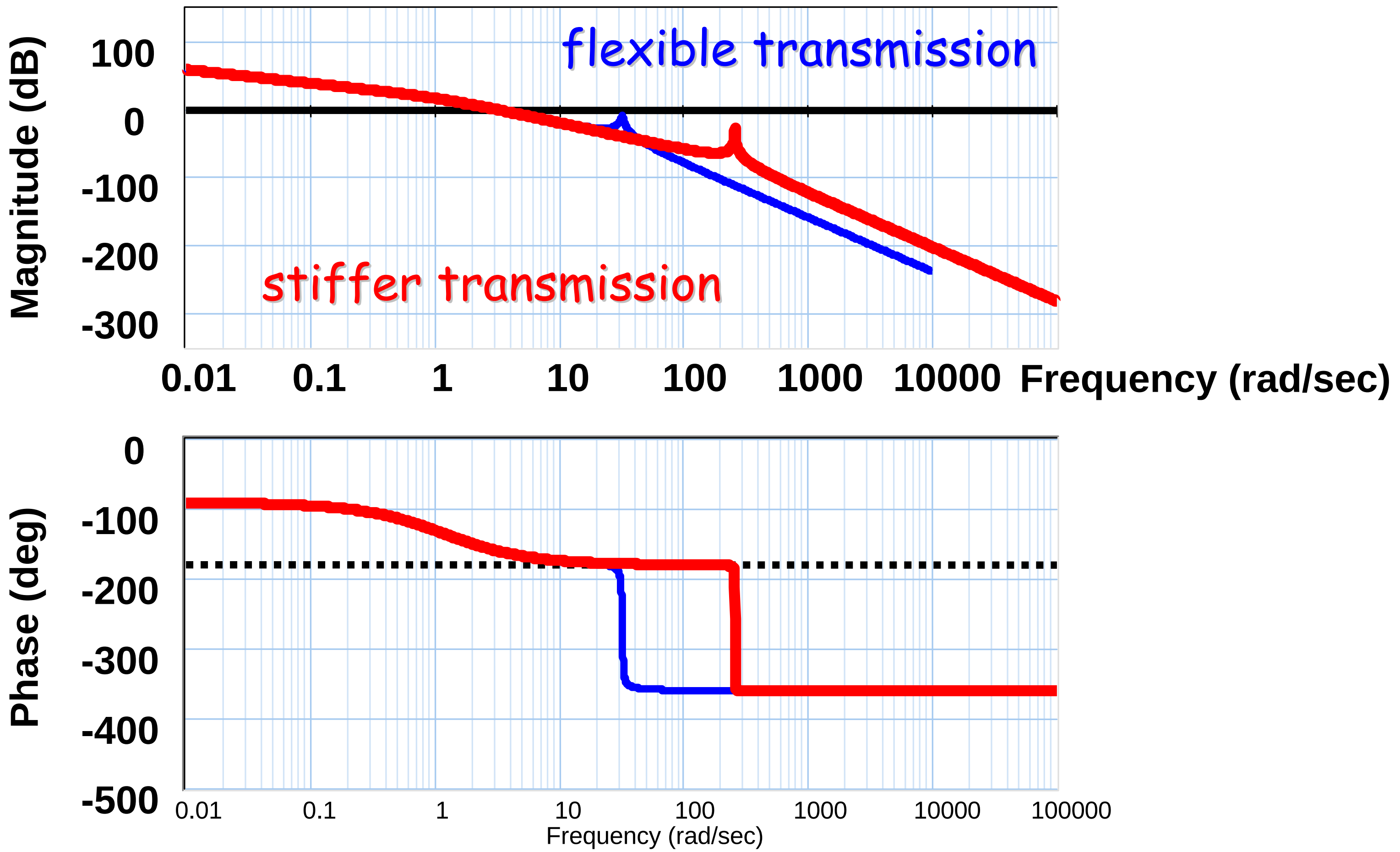


C_Prop_plus_Tacho_feedback_stiff_axis

Open loop comparison

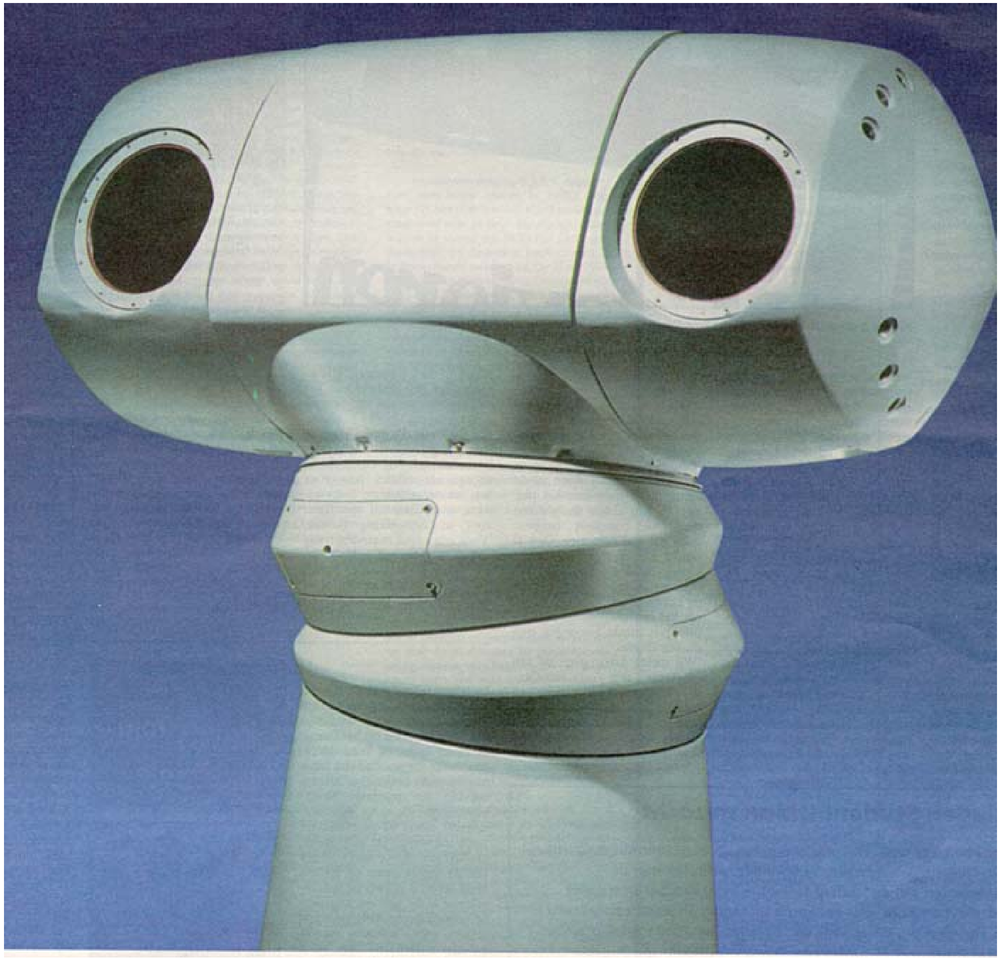


Bode plots

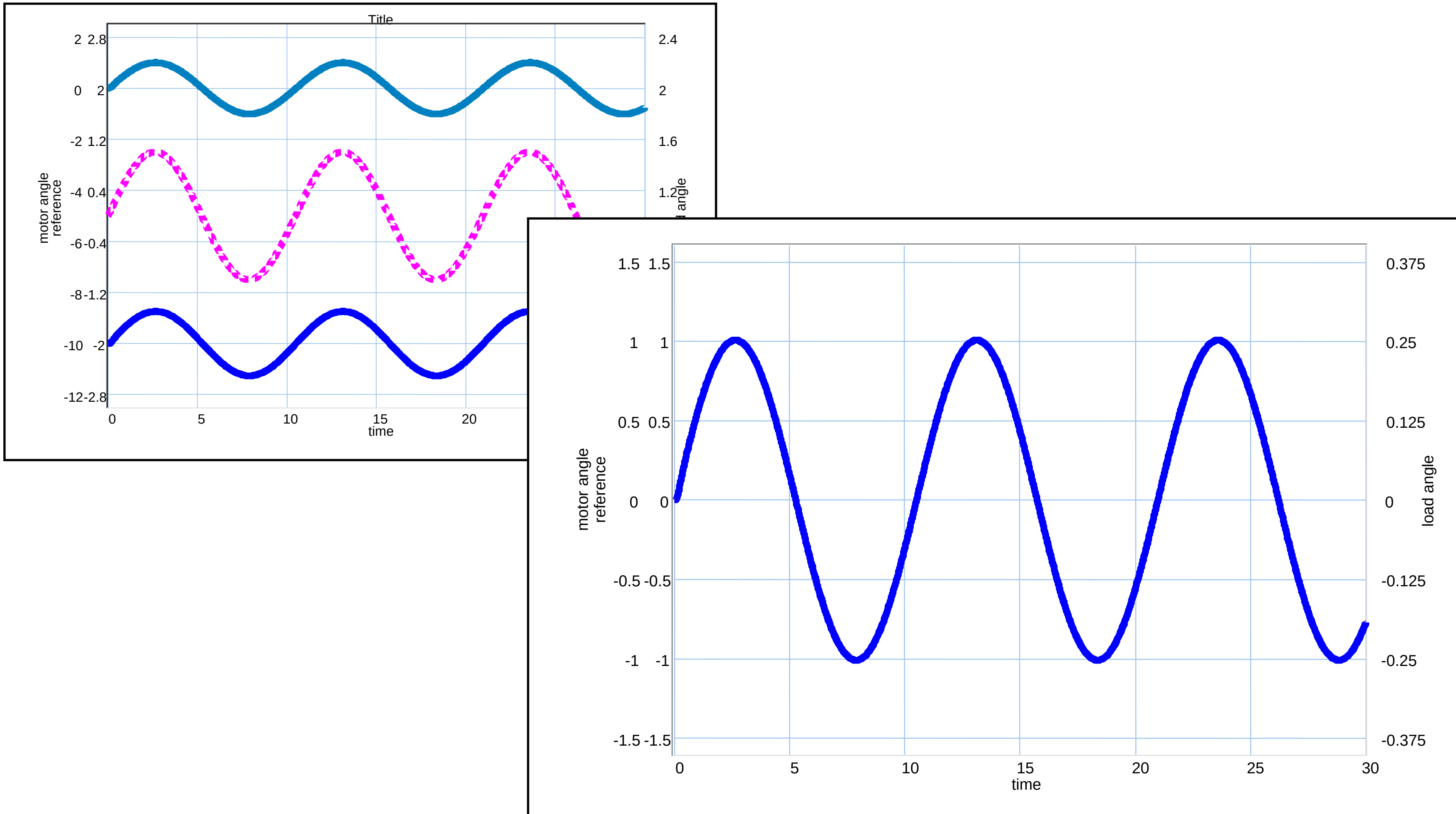

Magnitude (dB)
100
0
-100
-200
-300
flexible transmission
stiffer transmission
0.01
0.1
1
10
100
1000
10000
Frequency (rad/sec)
Phase (deg)
0
-100
-200
-300
-400
-500
0.01
0.1
1
10
100
1000
10000
100000
Frequency (rad/sec)

Tracking device

frequencies
sea waves
0.1 Hz
0.6 rad/s

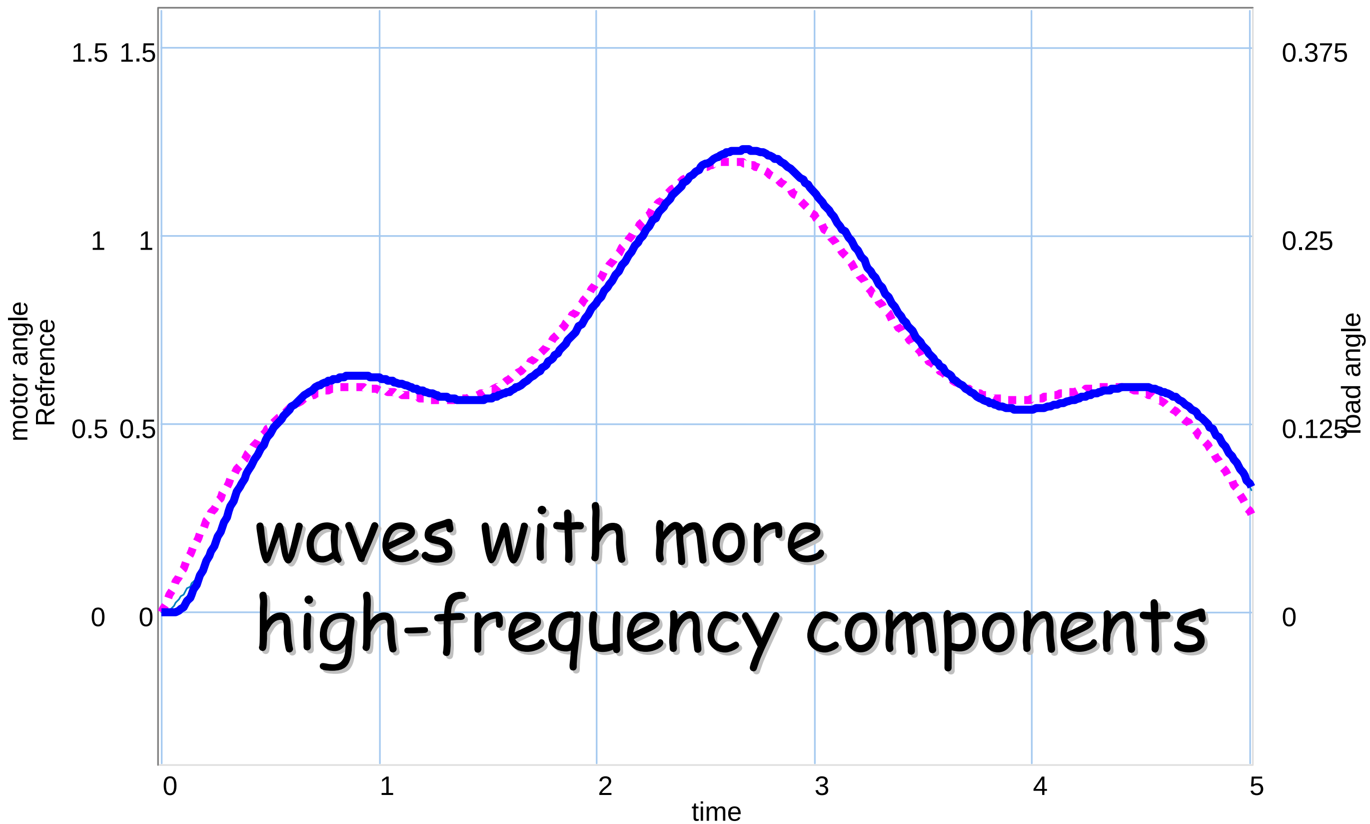


Responses

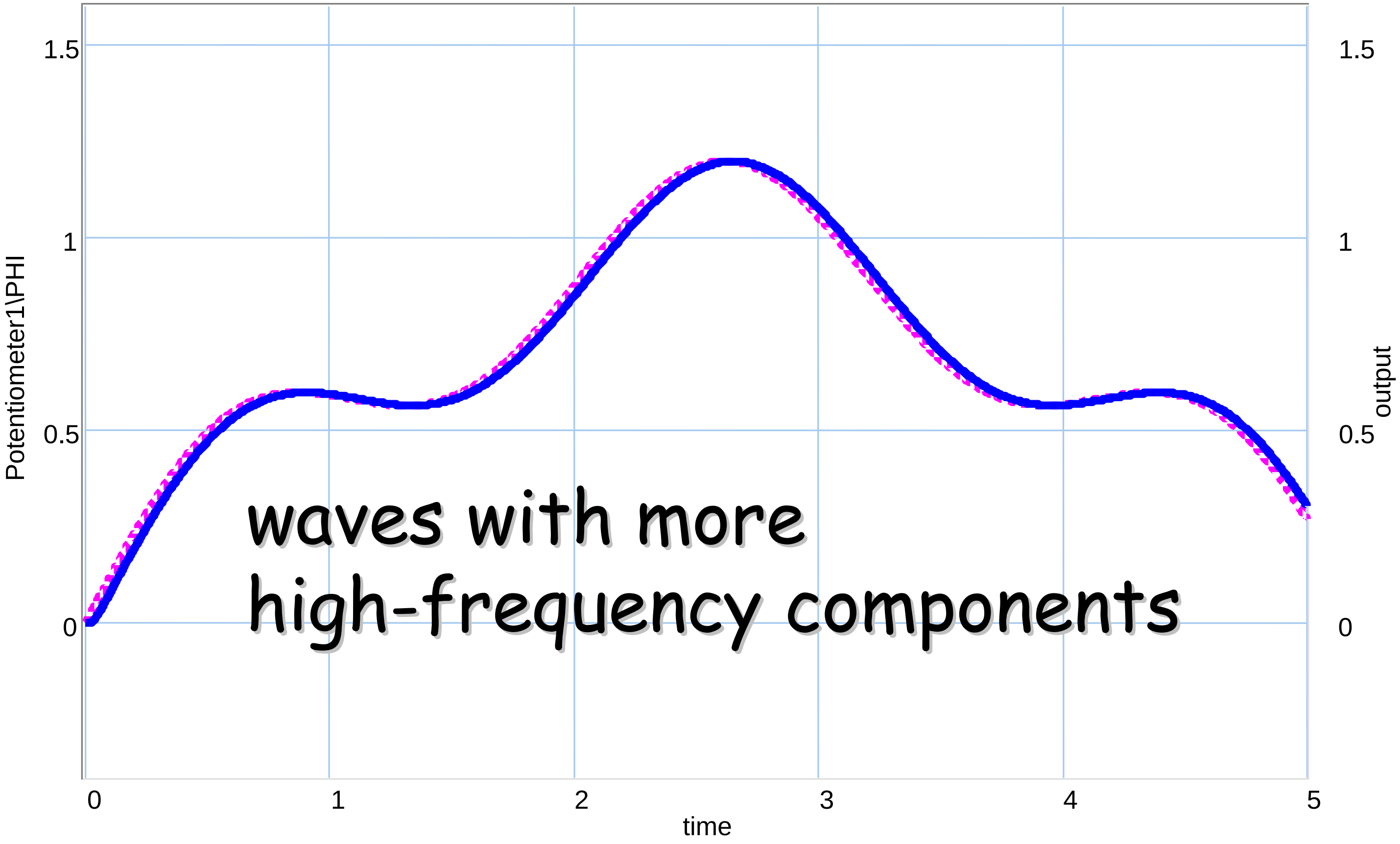

Title
2 2.8
0 2
-2 1.2
-4 0.4
-6 -0.4
-8 -1.2
-10 -2
-12 -2.8
2.4
2
1.6
1.2
motor angle
reference
0
5
10
15
20
time
1.5 1.5
1 1
0.5 0.5
0 0
-0.5 -0.5
-1 -1
-1.5 -1.5
0.375
0.25
0.125
0
-0.125
-0.25
-0.375
motor angle
reference
load angle
0
5
10
15
20
25
30
time

Bandwidth too small

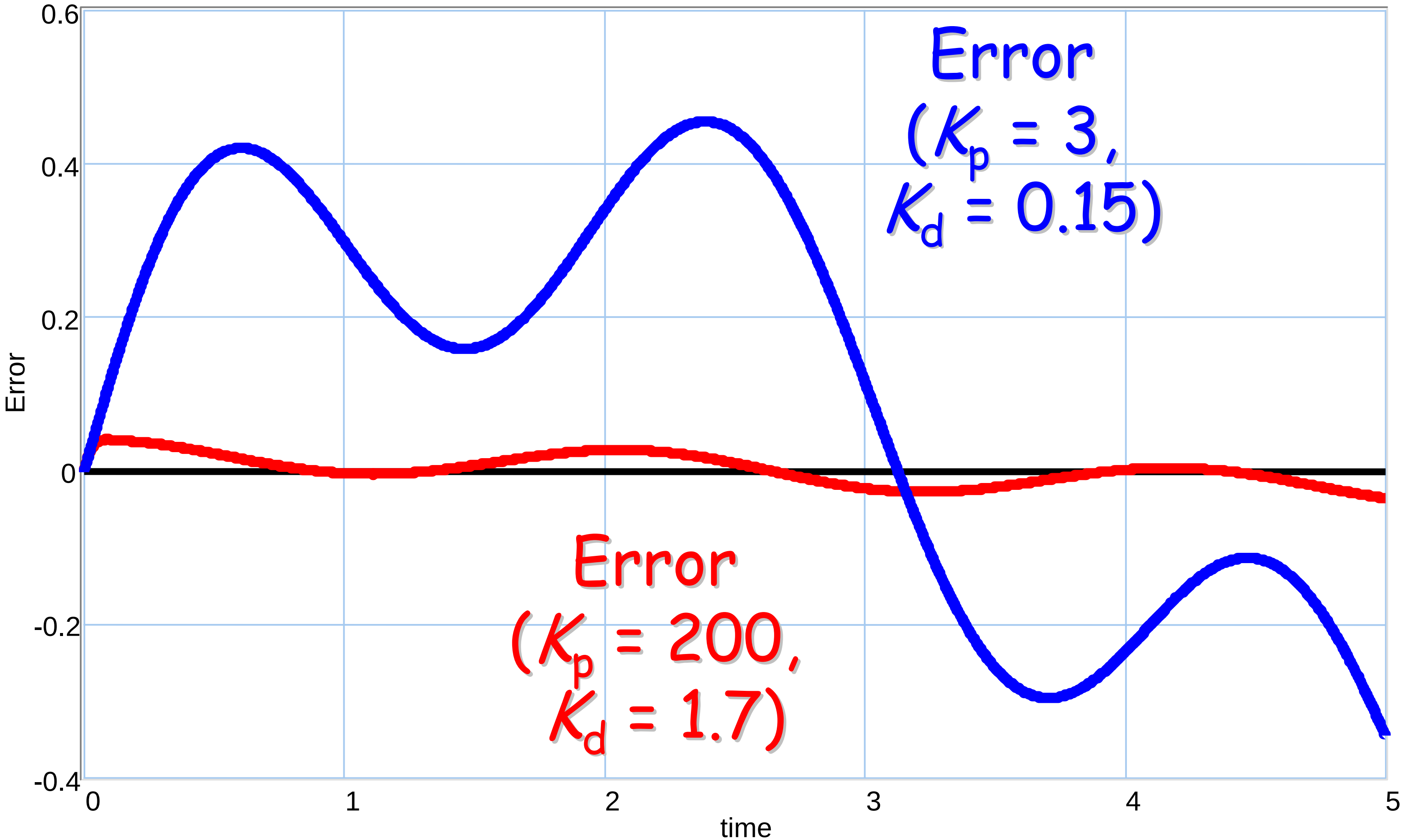
flexible transmission



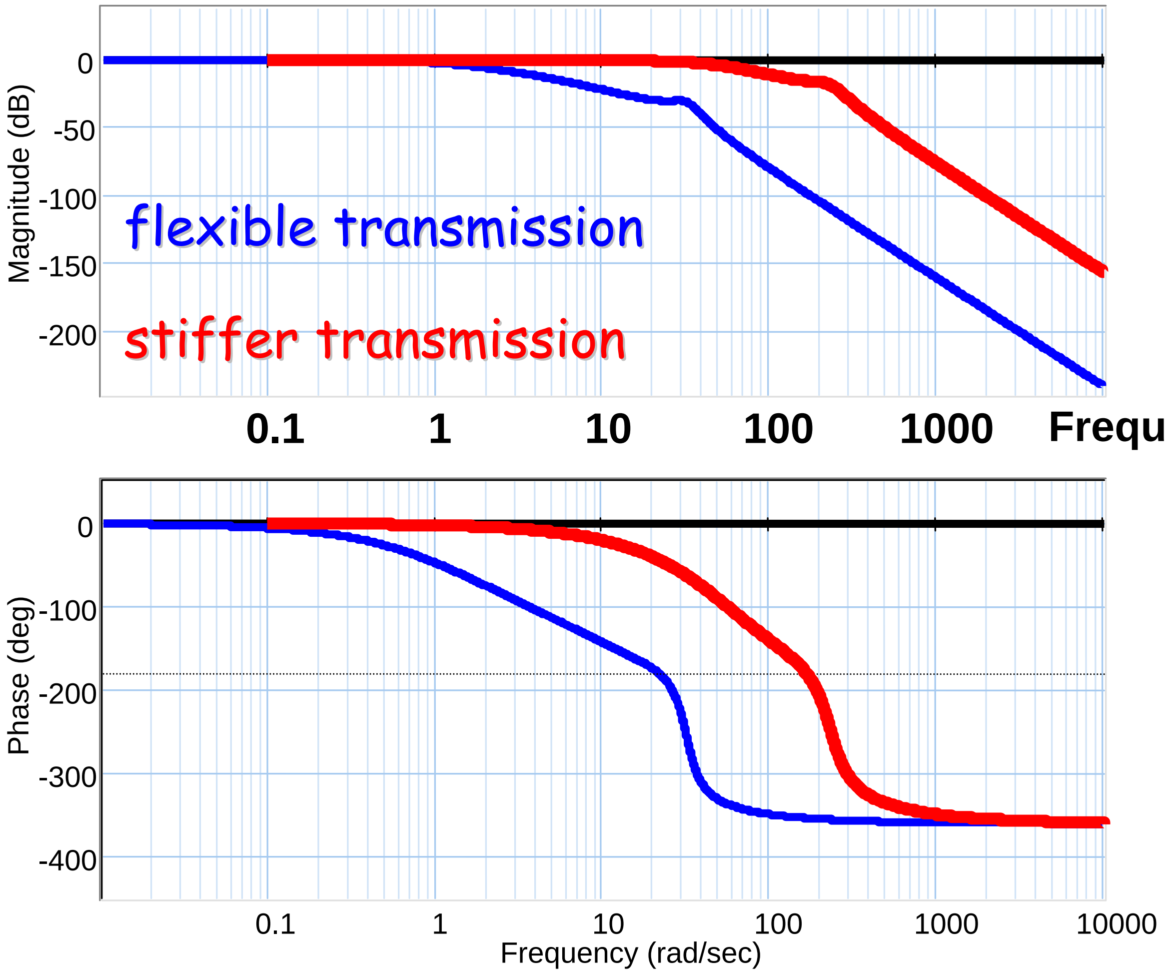
stiffer transmission



Comparison


0.6
0.4
0.2
0
-0.2
-0.4
Error
0
1
2
3
4
5
time
Error
(K_p = 3,
K_d = 0.15)
Error
(K_p = 200,
K_d = 1.7)

Closed-loop Bode plots



Bandwith:

1.2 rad/s

43 rad/s

Conclusions

- A realistic system can be controlled with the tools learned in this course

- What is left is the digital implementation of controllers:
  - Next two lectures

Mechatronica project

- Graag opgeven voor 14 maart